

### Land Use Planning and Approvals Act 1993

APPLICATION NO.

SA2023/019

LOCATION OF AFFECTED AREA

10 ALANAH COURT, OLD BEACH; 89 BASKERVILLE ROAD, OLD BEACH & 31 BASKERVILLE ROAD, OLD BEACH.

DESCRIPTION OF DEVELOPMENT PROPOSAL

**SUBDIVISION (3 LOTS PLUS BALANCE)** 

A COPY OF THE DEVELOPMENT APPLICATION MAY BE VIEWED AT <a href="https://www.brighton.tas.gov.au">www.brighton.tas.gov.au</a> AND AT THE COUNCIL OFFICES, 1 TIVOLI ROAD, OLD BEACH, BETWEEN 8:15 A.M. AND 4:45 P.M, MONDAY TO FRIDAY OR VIA THE QR CODE BELOW. ANY PERSON MAY MAKE WRITTEN REPRESENTATIONS IN ACCORDANCE WITH S.57(5) OF THE LAND USE PLANNING AND APPROVALS ACT 1993 CONCERNING THIS APPLICATION UNTIL 4:45 P.M. ON 08/07/2024. ADDRESSED TO THE GENERAL MANAGER AT 1 TIVOLI ROAD, OLD BEACH, 7017 OR BY EMAIL

AT

development@brighton.tas.gov.au.

REPRESENTATIONS SHOULD INCLUDE A DAYTIME TELEPHONE NUMBER TO ALLOW COUNCIL OFFICERS TO DISCUSS, IF NECESSARY, ANY MATTERS RAISED.

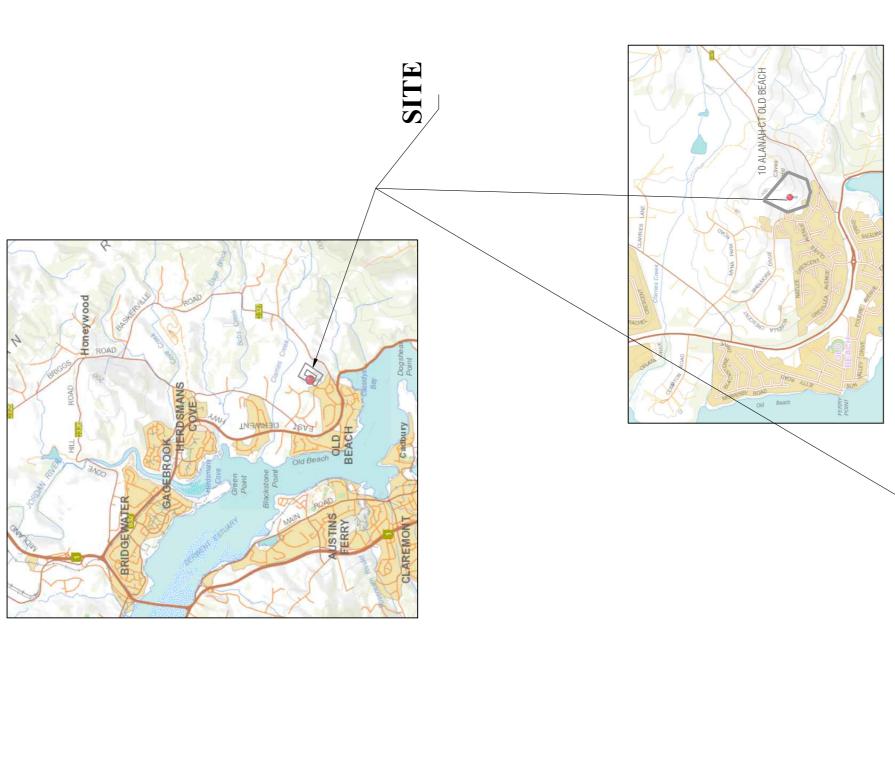
JAMES DRYBURGH General Manager





# LOCALITY SKETCH Not to Scale







NOT FOR CONSTRUCTION

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CLIENT:									

1. © THIS DRAWING IS PROTECTED BY COPYRIGHT AND SHALL NOT BE USED FOR ANY PURPOSE WITHOUT THE WRITTEN CONSENT OF INTEGRAL CONSULTING ENGINEERS.

2. THE LAYOUT OF ROADS AND SERVICES ARE SUBJECT TO CHANGE WITHOUT NOTICE.

3. LOT BOUNDARIES ARE SUBJECT TO CHANGE - REFER TO SURVEYOR'S PLANS FOR ACCURATE BOUNDARY LOCATIONS.

4. TAS NETWORKS AND TELSTRA SERVICES ARE NOT SHOWN. REFER TO TAS NETWORKS AND TELSTRA DRAWINGS BY OTHERS.

5. YOU MUST CONTACT DIAL BEFORE YOU DIG TO CHECK THE LOCATIONS OF ANY SITE SERVICES BEFORE WORK STARTS.

## GENERAL NOTES

- 1. BEFORE COMMENCING ANY EARTHWORKS YOU MUST CONTACT DIAL BEFORE YOU DIG 1100  $_{
  m e}$  REGARDING THE LOCATION OF UNDERGROUND ASSETS ON SITE
- 2. PRIOR TO COMMENCING WORKS, THE CONTRACTOR MUST SUBMIT AN APPLICATION FOR (WS02A) AND RECEIVE A PERMIT TO CONSTRUCT NEW TASWATER INFRASTRUCTURE
- 3. PIPE DEPTHS ARE SHOWN TO INVERT ONLY. ALLOW EXTRA 100MM DEPTH FOR BEDDING
- 4. ALL CONCRETE IS GRADE N25 U.N.O.
- . ALL WORKS TO COUNCIL STANDARD SPECIFICATIONS AND DRAWING U.N.O
- 6. CONNECTIONS TO EXISTING TASWATER AND COUNCIL SERVICES TO BE TO TASWATER AND COUNCIL STANDARDS AND APPROVAL
- 7. ALL AREAS OF FILL OR DISTURBANCE TO BE REINSTATED WITH MINIMUM OF 100MM OF APPROVED TOPSOIL & SEEDED WITH APPROVED SEED MIX
- 8. MARKERS TO BE PLACED FOR TELSTRA CONDUIT LOCATION UNDER ACCESSES
- 9. WATER CONNECTIONS TO EXISTING TAS WATER SERVICES TO BE UNDERTAKEN BY TASWATER AT DEVELOPER'S COST

# SOIL AND WATER MANAGEMENT

SOIL & WATER MANAGEMENT IS TO COMPLY WITH BEST PRACTICE TO PREVENT ANY TRANSFER OF SOIL MATERIAL OUTSIDE OF THE AREA SPECIFICALLY NECESSARILY DISTURBED FOR CONSTRUCTION OF THE SUBDIVISION. PARTICULAR ATTENTION SHALL BE PAID TO ENSURE THAT WATERIAL IS TRACKED ONTO ROADS & FOOTPATHS OR TO ENTER COUNCILS STORMWATER SYSTEM. ALL ASPECTS & PROTECTION MEASURES IN CONNECTION WITH SOIL & WATER MANAGEMENT ARE TO COMPLY WITH THE REQUIREMENTS COUNCILS DEVELOPMENT ENGINEER. THE CONTRACTOR SHALL SUBMIT A SOIL & WATER MANAGEMENT PLAN PRIOR TO STARTING WORK ON SITE.

REFER SOIL AND WATER MANAGEMENT CODE OF PRACTICE FOR HOBART AND REGIONAL COUNCILS.

# ROAD AND STORMWATER NOTES

- ALL WORKS TO BE UNDERTAKEN IN ACCORDANCE WITH THE TASMANIAN COUNCILS STANDARDS FOR SUBDIVISIONS AND IPWEA AND AWA STANDARD DRAWINGS WHERE APPLICABLE.
- 2. ALL SERVICES WITHIN THE ROAD RESERVATION TO BE LOCATED IN ACCORDANCE WITH TSD -G02
- 3. ALL PIPEWORK UNDER ROADS AND DRIVEWAYS TO BE BACKFILLED WITH FCR.
- 4. ALL SIDE ENTRY PITS TO BE CONSTRUCTED IN ACCORDANCE WITH TSD-SW09 OF TSD-SW10 UNLESS OTHERWISE APPROVED BY THE MUNICIPAL ENGINEER.

### SEWER NOTES

5. CONNECTIONS TO EXISTING SEWER MAINS TO BE CARRIED OUT BY TASWATER AT THE

## DEVELOPERS EXPENSE.

- 6. ALL MAINTENANCE STRUCTURES TO BE IN ACCORDANCE WITH WSA SEW1300 SERIES.
- . MANHOLE LIDS TO BE IN ACCORDANCE WITH AS3996:2006 & WSAA. CLASS 'D' IN ROAD RESERVES AND CLASS 'B' IN NON TRAFFICABLE AREAS.
- 8. PROVIDE 100Ø SEWER CONNECTION TO EACH LOT AS INDICATED ON THE PLAN. SEWER CONNECTION I.O'S TO BE RAISED TO THE SURFACE AND PROTECTED WITH A POLY COVER TO TASWATER APPROVAL PER STD DWG MRWA S-301 & 302 & TASWATER SEWER CODE SUPPLEMENT.
- 9. ALL PIPEWORK UNDER ROADS, DRIVEWAYS AND TRAFFICABLE AREAS TO BE BACKFILLED WITH FCR IN ACCORDANCE WITH STD DWG MRWA-S-201. TRAFFICABLE COVERS TO MRWA SECT 4 15 2
- 10. ALL WORKS TO BE IN ACCORDANCE WITH THE SEWERAGE CODE OF AUSTRALIA WSA 02-2014-3.1 MRWA VERSION 2.0 & TASWATER SUPPLEMENT.
- 11. ALL WORKS MUST BE INSPECTED AND TESTED BY TASWATER PRIOR TO BACKFILL.
- 12. MINIMUM PIPE COVER TO BE PER STD DWG MRWA-S-201 OF THE SEWERAGE CODE OF AUSTRALIA WSA 02-2014-3.1 MRWA VERSION 2.0
- CLEARANCES BETWEEN SEWER & OTHER UNDERGROUND SERVICES TO BE IN ACCORDANCE WITH WSA 02-2014-3.1 MRWA VERSION 2.0 TABLE 4.2

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### WATER NOTES

- 1. CONNECTIONS TO EXISTING WATER MAINS TO BE CARRIED OUT BY TASWATER AT DEVELOPERS EXPENSE.
- HOUSE CONNECTION TO EACH LOT TO BE DN25 PE 100 PN 16 PIPE AS INDICATED ON THE PLANS. IN ACCORDANCE WITH TWS-W-0002. EACH LOT IS TO BE SUPPLIED WITH AN INDIVIDUAL 20MM DIAMETER METER WITH INTEGRAL DUAL CHECK VALVE AND GATE VALVE WITH A PVC BOX AS SPECIFIED BY TASWATER.
- DETECTOR TAPE IS TO BE INSTALLED OVER ALL NON-METALLIC WATER MAINS.
- 4. ALL FIRE HYDRANT COMPONENTS TO BE DN100
- 5. HYDRANT ROAD MARKING INDICATORS SHALL BE INSTALLED IN ACCORDANCE WITH SEC.8 IPWEA TAS "FIRE HYDRANT GUIDELINES"
- ALL PIPEWORK UNDER ROADS AND DRIVEWAYS TO BE BACKFILLED WITH FCR IN ACCORDANCE WITH WAT-1201-V.

6

- ALL WORKS MUST BE TO THE WATER SUPPLY CODE OF AUSTRALIA WSA 03 -2011-3.1
  VERSION 3.1 MRWA EDITION V2. AND TASWATER'S SUPPLEMENTS, TASWATER'S
  STANDARD DRAWINGS TW-SD-W-20 SERIES, WATER METERING POLICY / METERING
  GUIDELINES, BOUNDARY BACKFLOW CONTAINMENT REQUIREMENTS & AS3500.1:2003.
- 8. WATER MAINS >= 100mm TO BE mPVC OR oPVC TYPE 2 CLASS 16 PIPE OR <100mm TO

## BE PE PIPE CLASS 16.

- 9. ALL WORKS MUST BE INSPECTED AND TESTED BY TAS WATER PRIOR TO BACKFILL.
- 10. MINIMUM PIPE COVER TO BE PER TABLE 5.4.2.1 OF TAS WATER SUPPLEMENT TO WATER SUPPLEMENT. SUPPLY CODE OF AUSTRALIA WSA V3.1 03-2011 & TAS WATER SUPPLEMENT.
- 11. THRUST BLOCKS TO BE IN ACCORDANCE WITH WATER SUPPLY CODE OF AUSTRALIA WSA V3.1 03-2011
- 12. FOR WATERMAINS OF 200MM DIA OR LESS THE HORIZONTAL CLEARANCE TO OTHER SERVICES OR SERVICE STRUCTURES SHALL BE PROVIDED IN ACCORDANCE WITH WSA 03-2011-3.1 MRWA ED VERS 2 AND TASWATER SUPPLEMENT.

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## GENERAL LOT 3 993m<sup>2</sup> FUTURE LOT LAYOUT DRAFT ONLY FOR DISCUSSION PROPOSED LOT LAYOUT LOT 2 923m<sup>2</sup> LOT 1 783m² COURT MANAH

## NOTES

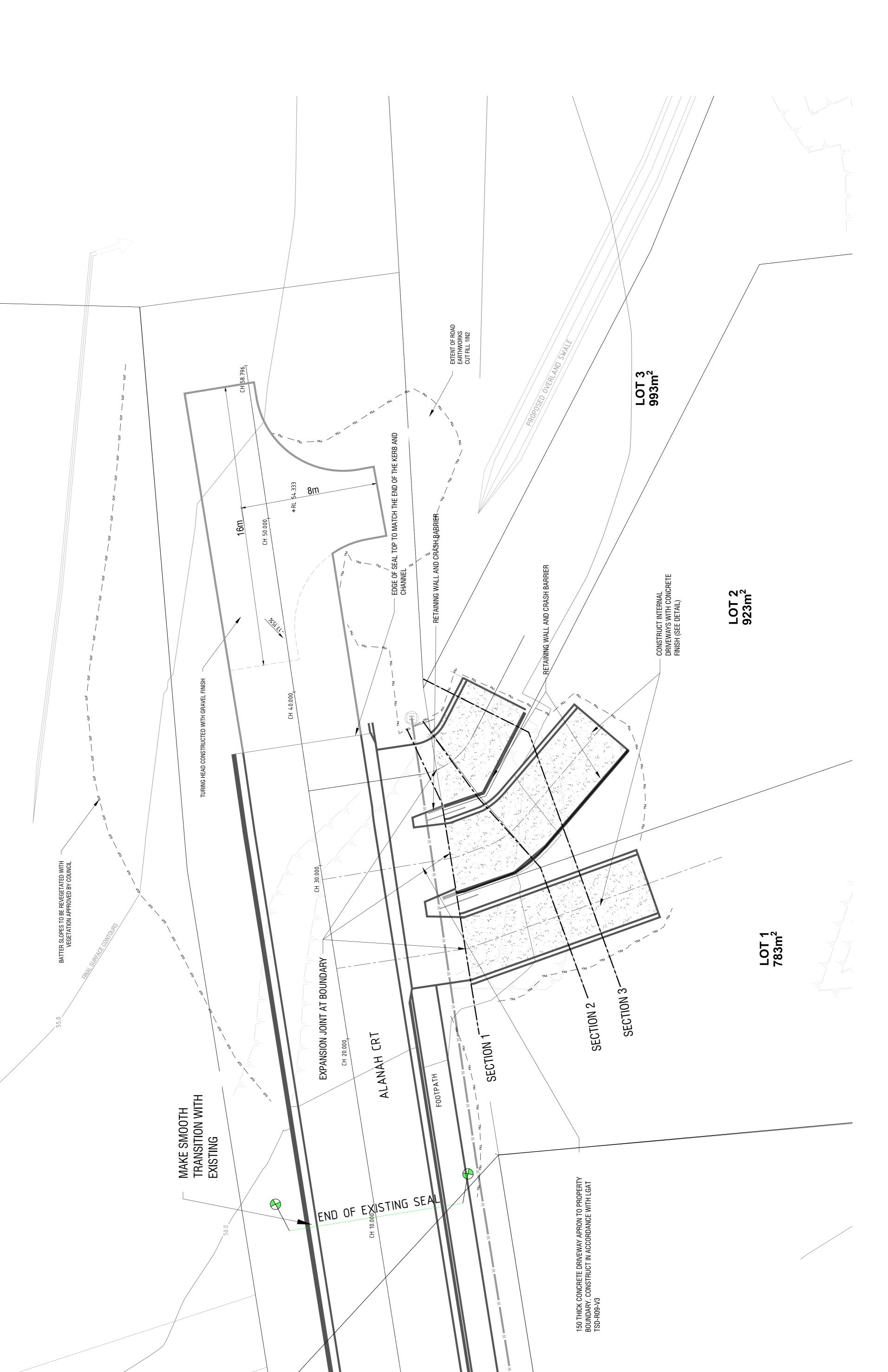
LAYOUT OF FUTURE LOTS IS FOR DISCUSSION PURPOSES ONLY.

ROAD ALIGNMENT AND LOT LAYOUT SHOWN MAY CHANGE IN THE FUTURE AND ONLY TO BE TAKEN IN CONSIDERATION FOR ACCESSIBILITY FROM ALANAH COURT.

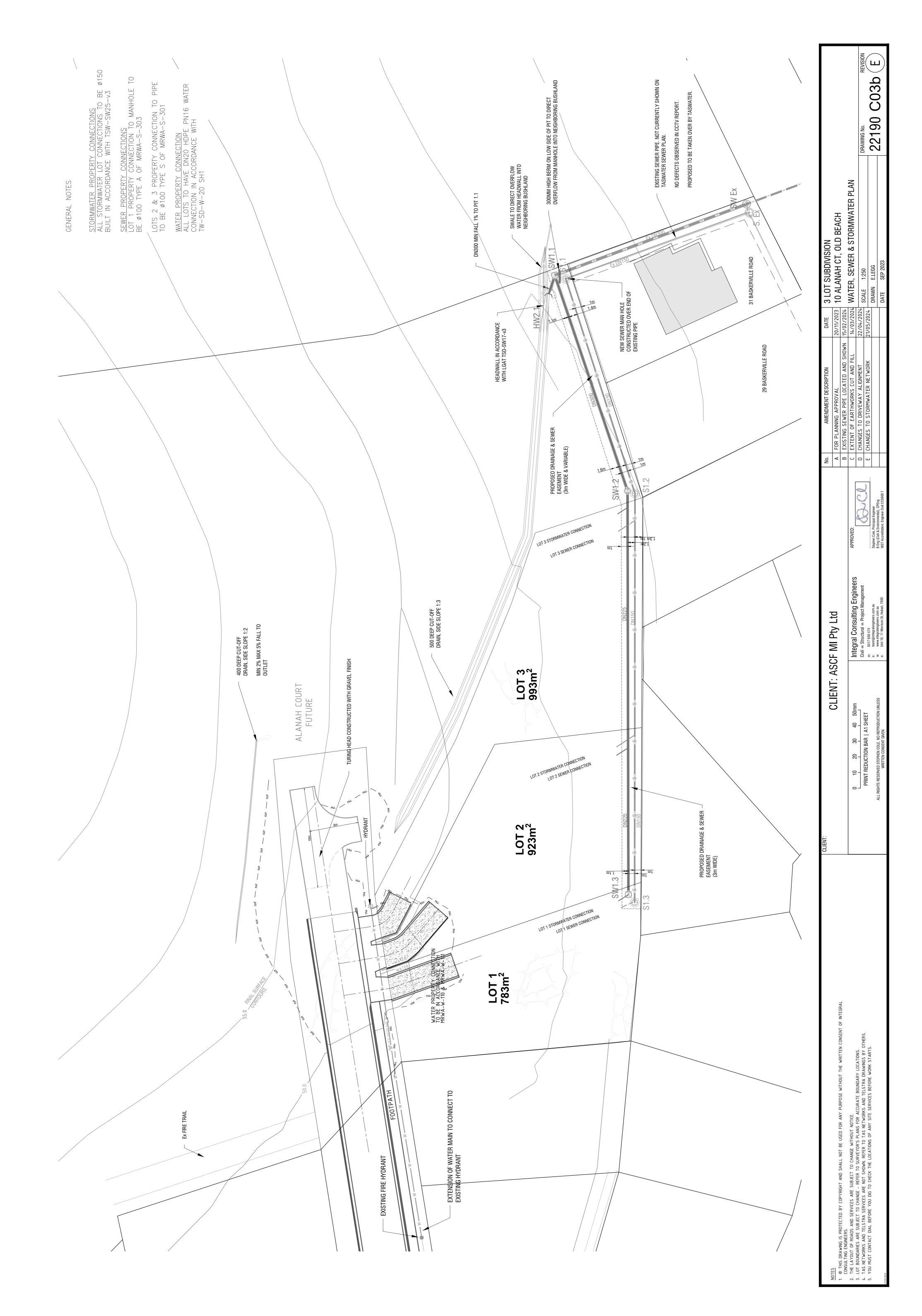
EXTENSION OF ALANAH COURT TO OCCUR AS FAR AS TURNING HEAD, SEE SHEET 5 FOR DETAILS.

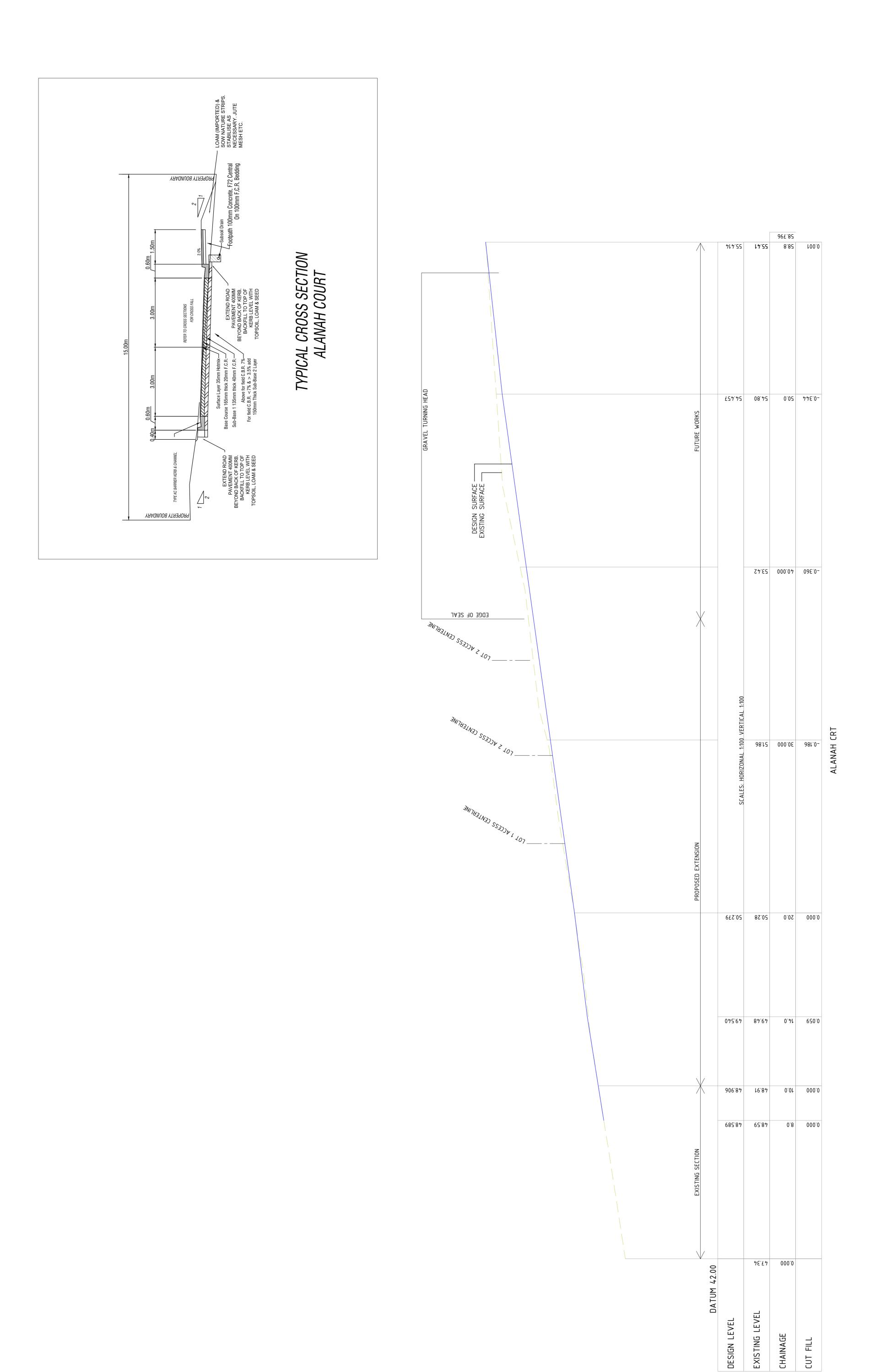
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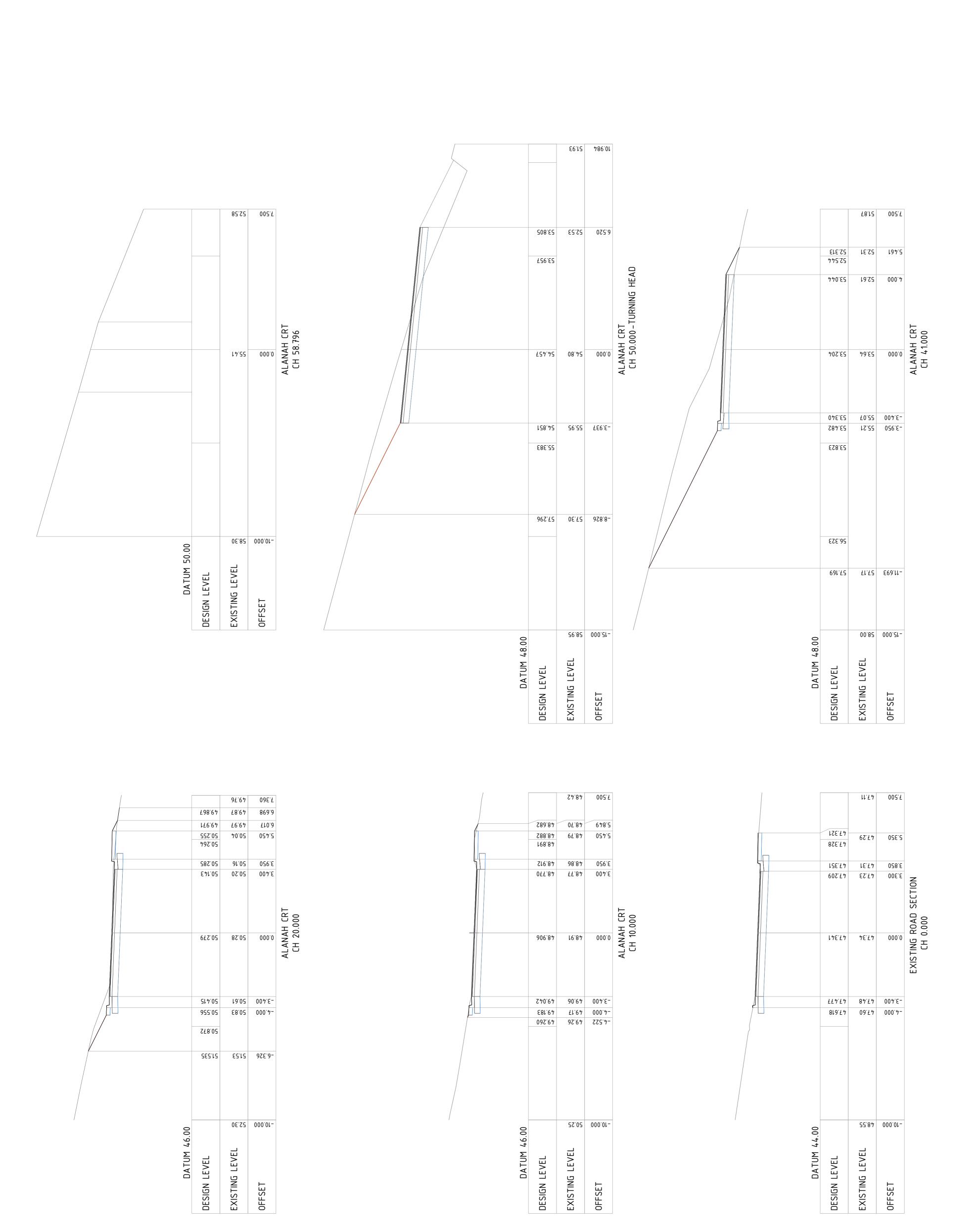


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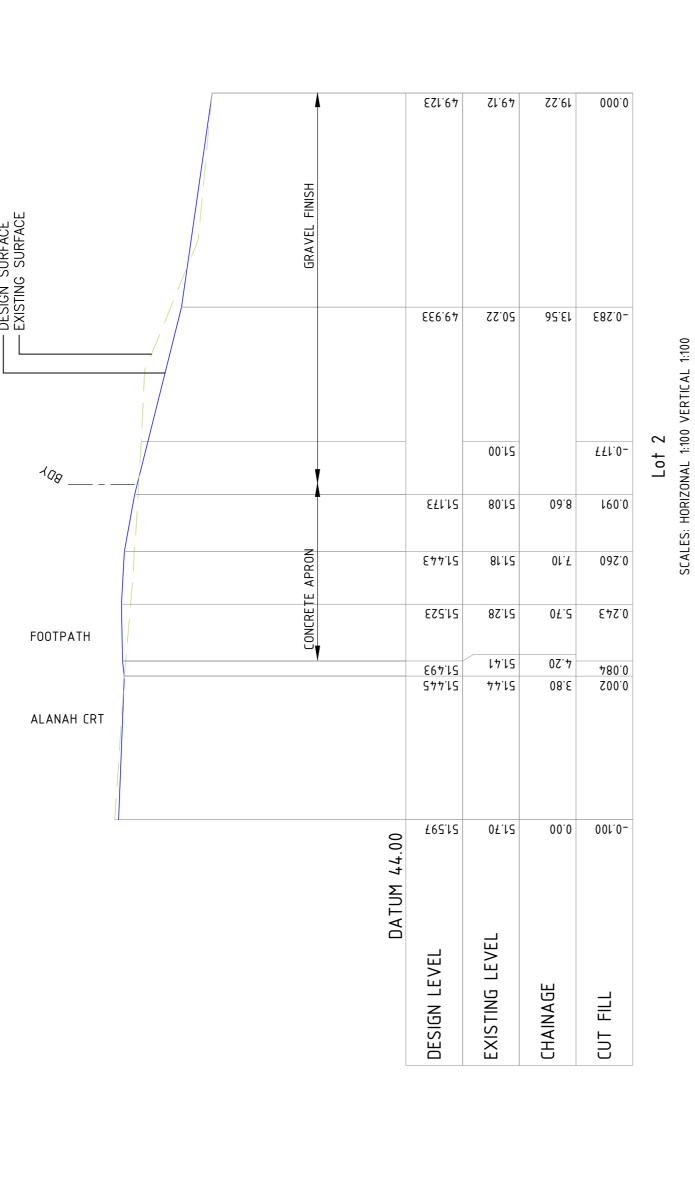


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CLIENT: THIS DRAWING IS PROTECTED BY COPYRIGHT AND SHALL NOT BE USED FOR ANY PURPOSE WITHOUT THE WRITTEN CONSENT OF INTEGRAL  SCHILL THIS ENGINEEDS.	E LAYOUT OF ROADS AND SERVICES ARE SUBJECT TO CHANGE WITHOUT NOTICE.  T BOUNDARIES ARE SUBJECT TO CHANGE – REFER TO SURVEYOR'S PLANS FOR ACCURATE BOUNDARY LOCATIONS.	S NETWORKS AND TELSTRA SERVICES ARE NOT SHOWN. REFER TO TAS NETWORKS AND TELSTRA DRAWINGS BY OTHERS. U MUST CONTACT DIAL BEFORE YOU DIG TO CHECK THE LOCATIONS OF ANY SITE SERVICES BEFORE WORK STARTS.	



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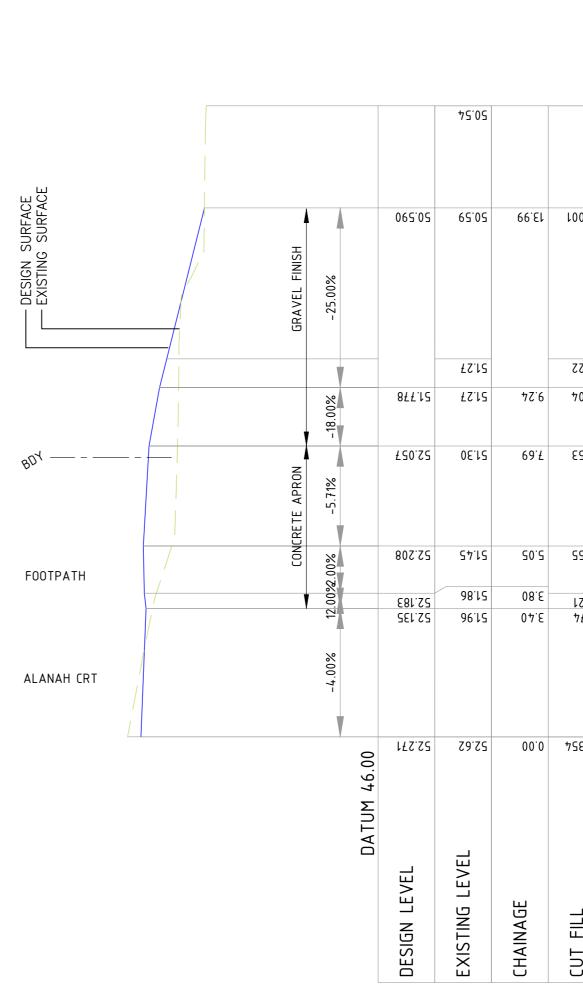
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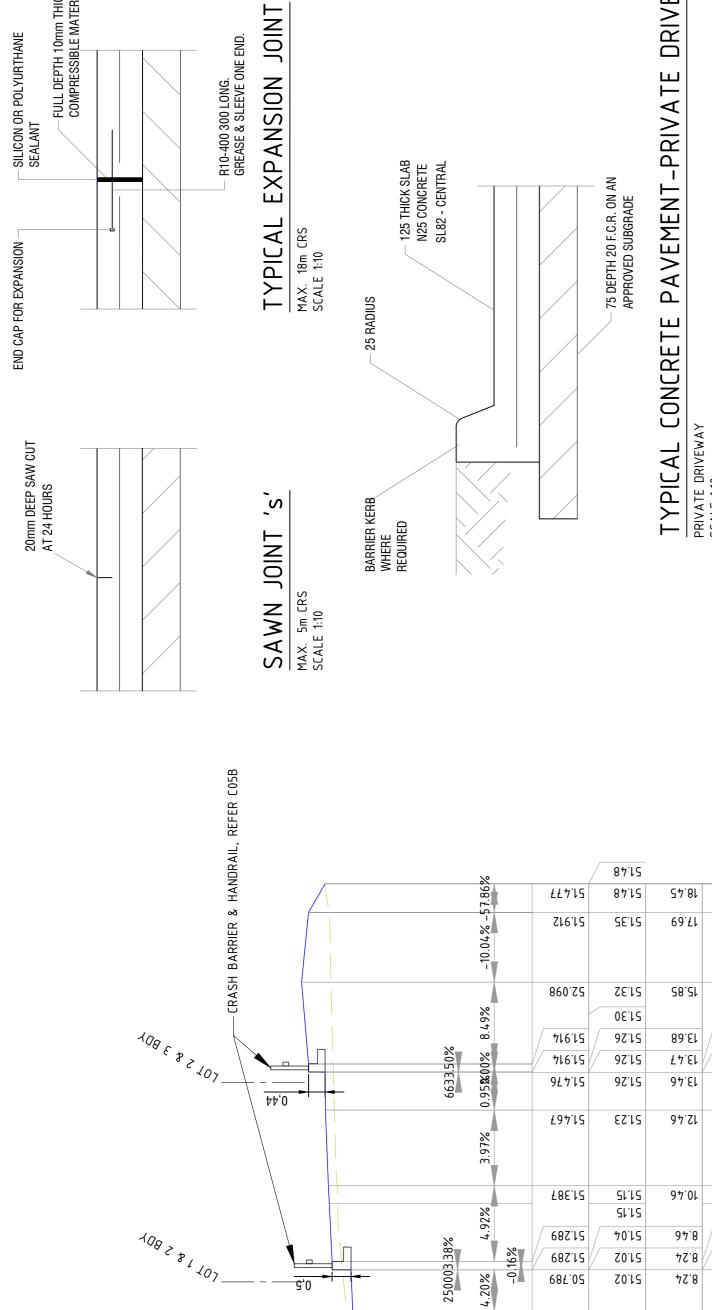
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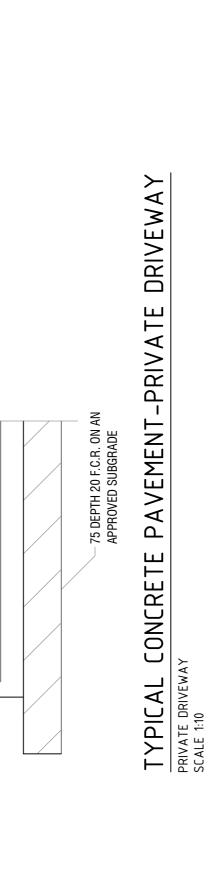
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FULL DEPTH 10mm THICK COMPRESSIBLE MATERIAL

SILICON OR POLYURTHANE SEALANT



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**DATUM 46.00** 

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EXISTING LEVEL

CHAINAGE

CUT FILL

DESIGN LEVEL

0.655 81.02 42.8 524.0

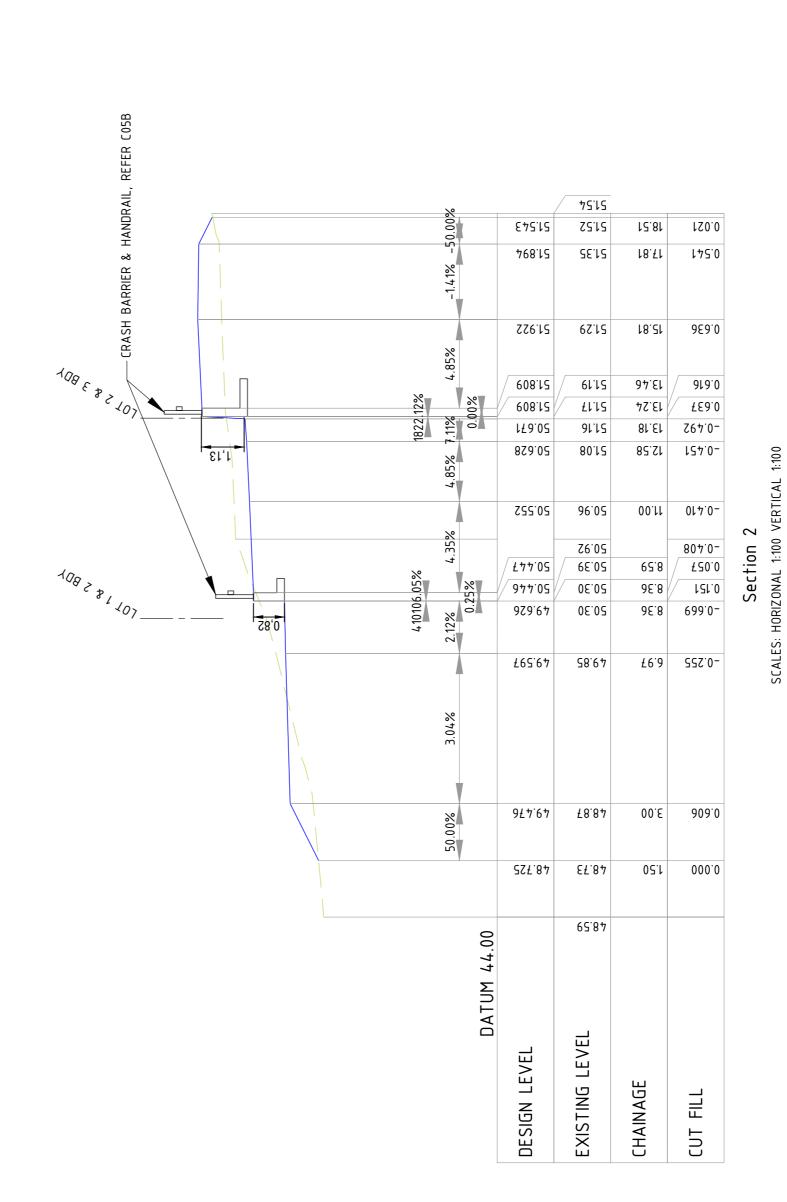
Section 1

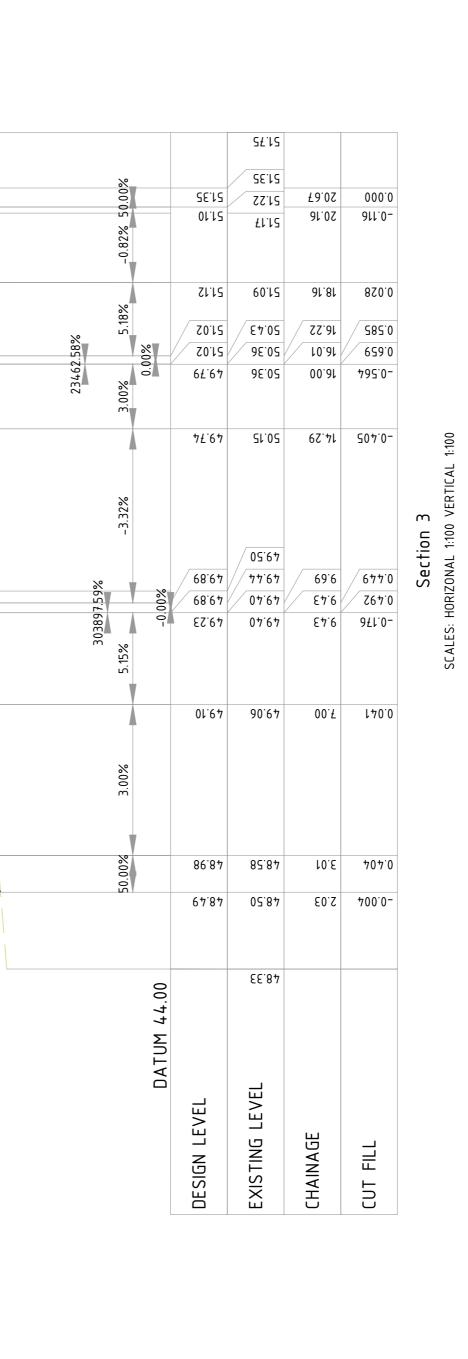
CRASH BARRIER & HANDRAIL, REFER C05B

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3 LOT SUBDIVISION	14/03/2024 10 AI ANAH CT. OI D BFACH		22/04/2024 VEHICLE ACCESS CROSS SECTION	SCALE 1:100	SUALE 1.100	DRAWN E.LEGG	DATE SEP 2023
DATE	14/03/2024	18/03/2024	22/04/2024	•			
No. AMENDMENT DESCRIPTION	A FOR PLANNING APPROVAL	C DRAFT FOR COUNCIL COMMENT	D CHANGES TO DRIVEWAY ALIGNMENT				
			APPROVED:		3	Stephen Cole, Principal Engineer	B Eng (UMI & EnVironmental), UPEng WST Accreditation: Engineer Civil CC5900 T
	ENT. ASCFIVI PLY LLC		Integral Consulting Engineers	Civil ∞ Structural ∞ Project Management			w. www.nitegratenigmets.contr.au a: Unit 10, 11 Morrison St, Hobart, 7000
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CROSS SECTIONS

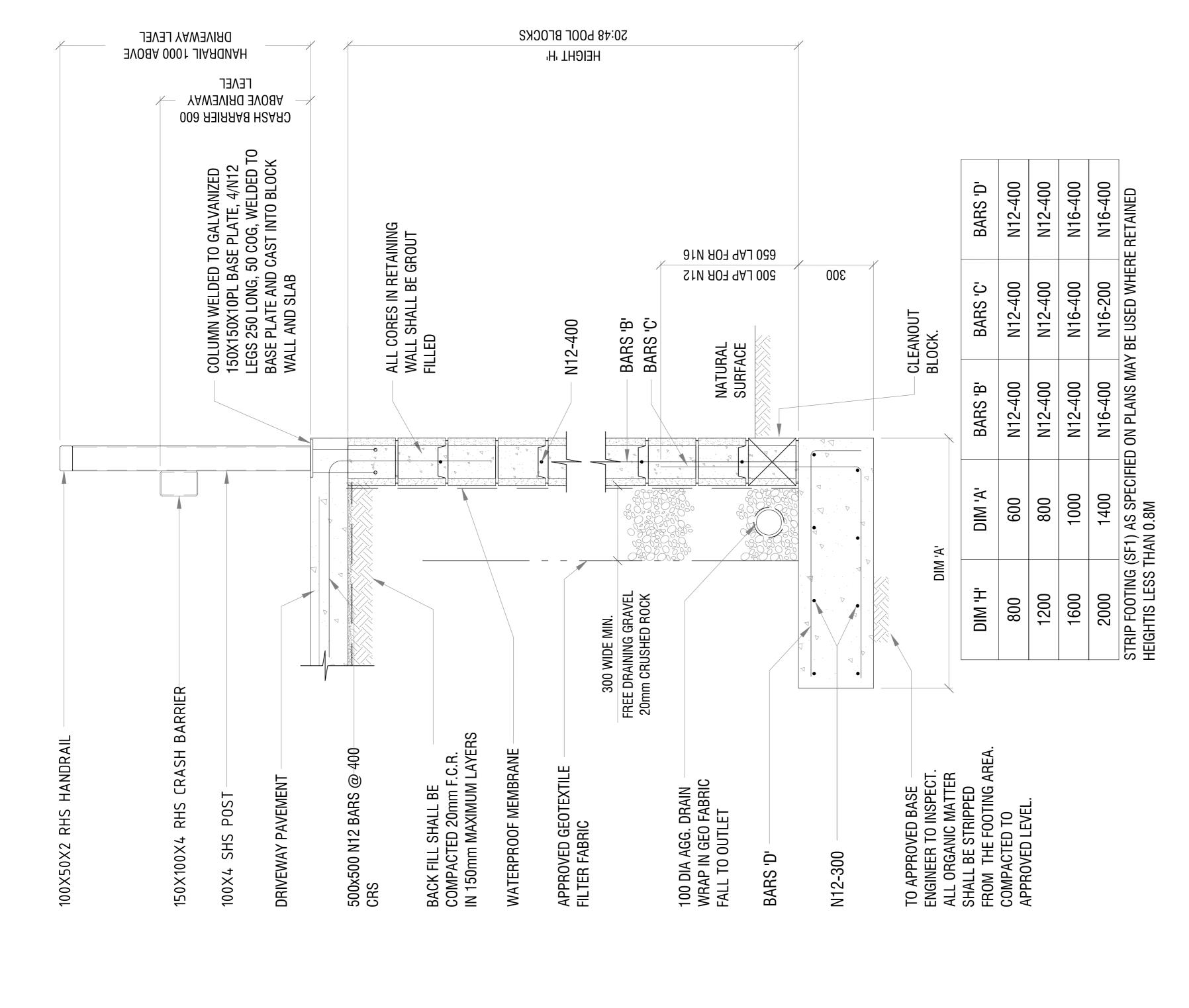
# TION NOTES RETAINING WALL CONSTRUC

- MORTAR SHALL BE CEMENT: LIME: SAND RATIO THUS:1:0-0.25:3 BLOCKS TO BE GRADE 12 TO A.S. 2733 GROUT MAX. AGGREGATE SIZE 10mm SLUMP 230 +/-30 MIN.
  - CHARACTERISTIC STRENGTH 20 MPa.
- RETAINING WALL FOOTINGS ARE TO BE FOUNDED ON APPROVED TRIMMED SUBGRADE WITH A MIN. BEARING CAPACITY OF 150 KPa. CONCRETE STRENGTH(MPa)/SLUMP(mm) FOOTINGS 25/90 50 COVER TO FOOTING BASE REINFORCEMENT ALL CORES SHALL BE GROUT FILLED TO ONE COURSE ABOVE FINISHED SURFACE LEVEL. CLEANOUT HOLES ARE TO BE PROVIDED TO THE BASE OF ALL CORES. AT THE END OF EACH DAYS BLOCK LAYING, & BEFORE THE WALL IS FILLED, MORTAR DROPPINGS ARE TO BE WASHED OUT REINFORCEMENT TIED AND HOLES BLOCKED OFF.
  - 5.

~ .

6.

- ALLOW MIN. 14 DAYS AFTER FILLING BLOCKS PRIOR TO BACKFILLING BEHIND WALL. <u>ල</u>
- CORE FILL TO BE PLACED WITH A PENCIL VIBRATOR.
   MOIST CURE WALL CONCRETE FOR 14 DAYS PRIOR TO WATERPROOFING.
   BACK OF WALL TO BE COATED WITH MIN. 2 COATS OF AN APPROVED BITUMINOUS PAINT, LINED WITH FORTECON PROTECTED BY COREFLUTE OR SIMILAR SACRIFICIAL SHEETING.
  - 13. PROVIDE EXPANSION JOINTS AT MAX. 10m CRS. PROVIDE R10 DOWEL BARS ACROSS JOINTS AT 400 CRS., GREASED AND CAPPED ONE END



ORCING LAP	LAP LENGTH U.N.O.	200	029	008	1000	1150	1300	1450
REINFORCING	SIZE	N12	N16	N20	N24	N28	N32	N36

### - RW1 **RETAINING WAL SCALE 1:10**

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3 LOT SUBDIVISION	10 ALANAH CT. OLD BFACH		4 CRASH BARRIER DETAIL	1:40	SCALE I.10	- DRAWN E.LEGG	DATE SEP 2023
DATE	14/03/2024	18/03/2024	21/05/2024				
No. AMENDMENT DESCRIPTION	A FOR PLANNING APPROVAL	C DRAFT FOR COUNCIL COMMENT	D CRASH BARRIER DETAIL				
			APPROVED:		3	Stephen Cole, Principal Engineer	B Eng (Civil & Environmental), CPEng WST Accreditation: Engineer Civil CC5900 T
1 + 1 - 1 1 N 1 O V	OLIENT: ASOF IVII PLY LLA		Integral Consulting Engineers	Civil ∞ Structural ∞ Project Management		m: U417 650 474 e: team@integralengineers.com.au	w: www.integralengineers.com.au a: Unit 10, 11 Morrison St, Hobart, 7000
LIVLI	CLIENI		0 10 20 30 40 50mm		PRINT REDUCTION BAR   A1 SHEET		ALL RIGHTS RESERVED STEPHEN COLE. NO REPRODUCTION UNLESS WRITTEN CONSENT GIVEN
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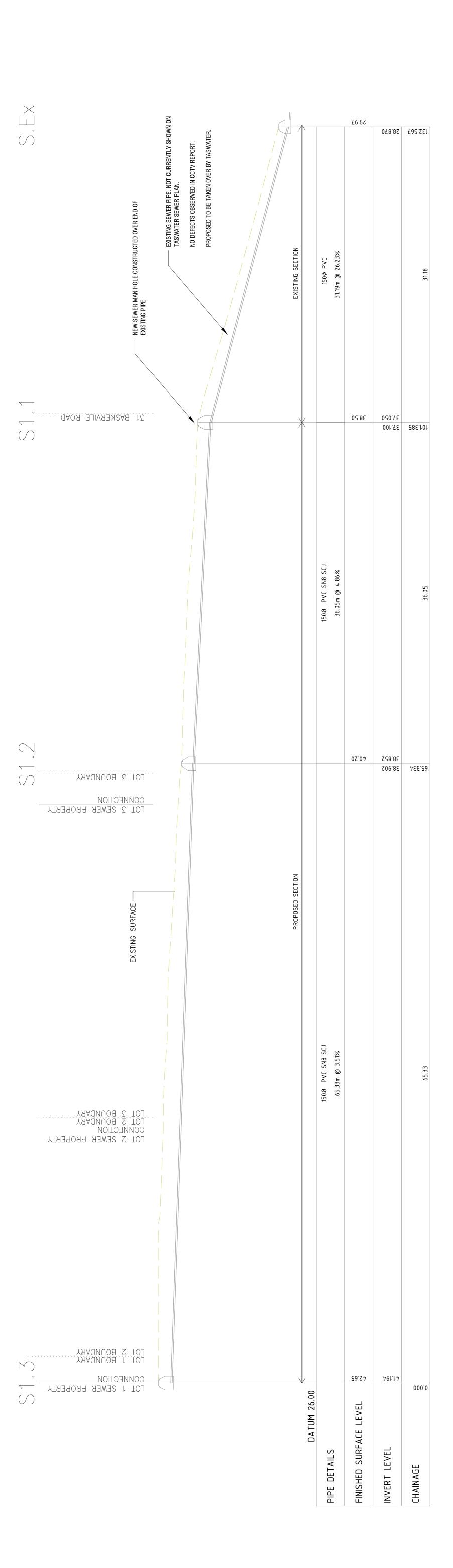
1. © THIS DRAWING IS PROTECTED BY COPYRIGHT AND SHALL NOT BE USED FOR ANY PURPOSE WITHOUT THE WRITTEN CONSENT OF INTEGRAL CONSULTING ENGINEERS.

2. THE LAYOUT OF ROADS AND SERVICES ARE SUBJECT TO CHANGE WITHOUT NOTICE.

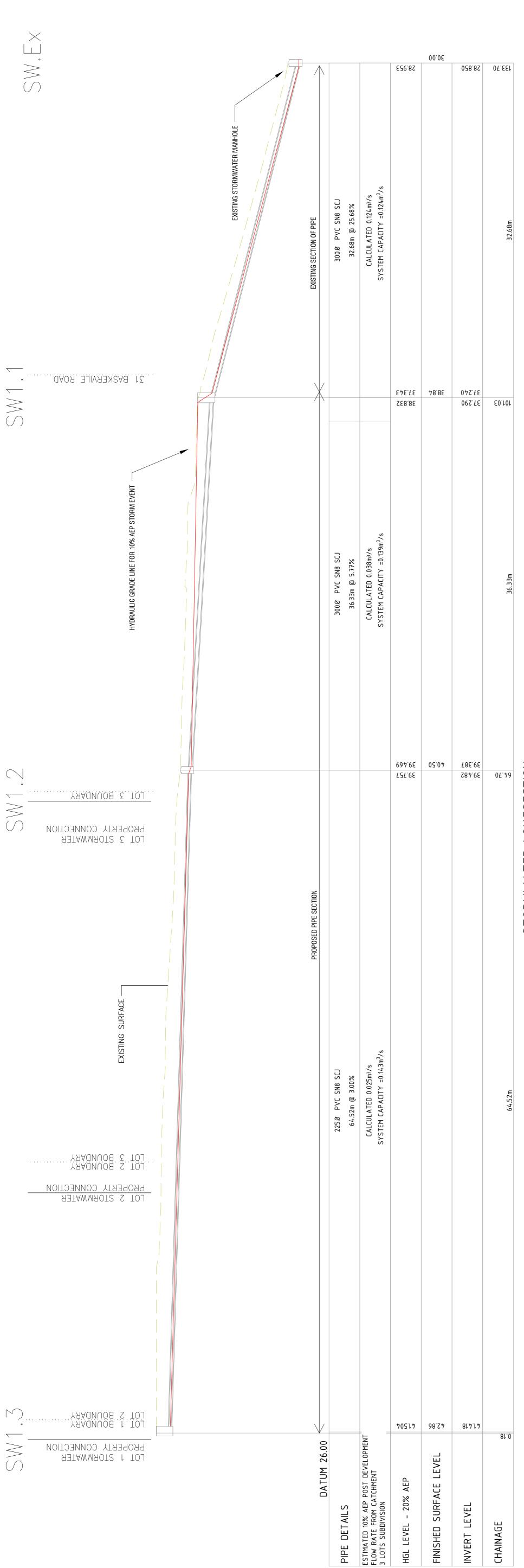
3. LOT BOUNDARIES ARE SUBJECT TO CHANGE - REFER TO SURVEYOR'S PLANS FOR ACCURATE BOUNDARY LOCATIONS.

4. TAS NETWORKS AND TELSTRA SERVICES ARE NOT SHOWN. REFER TO TAS NETWORKS AND TELSTRA DRAWINGS BY OTHERS.

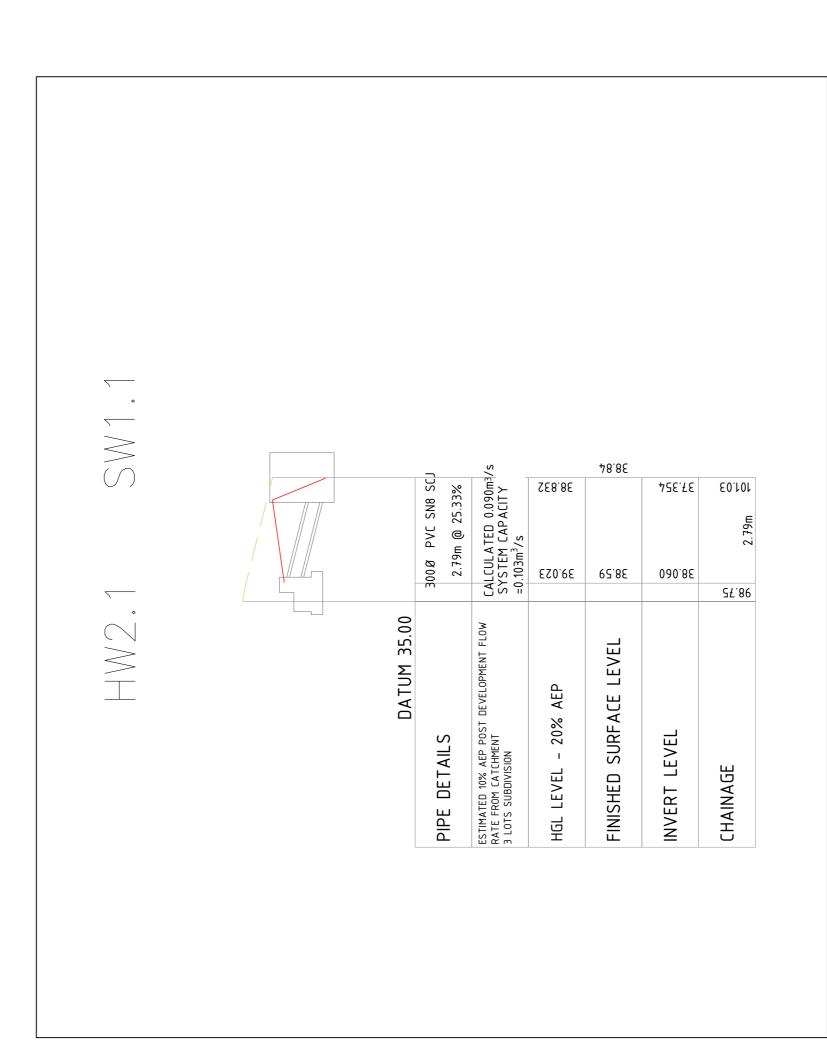
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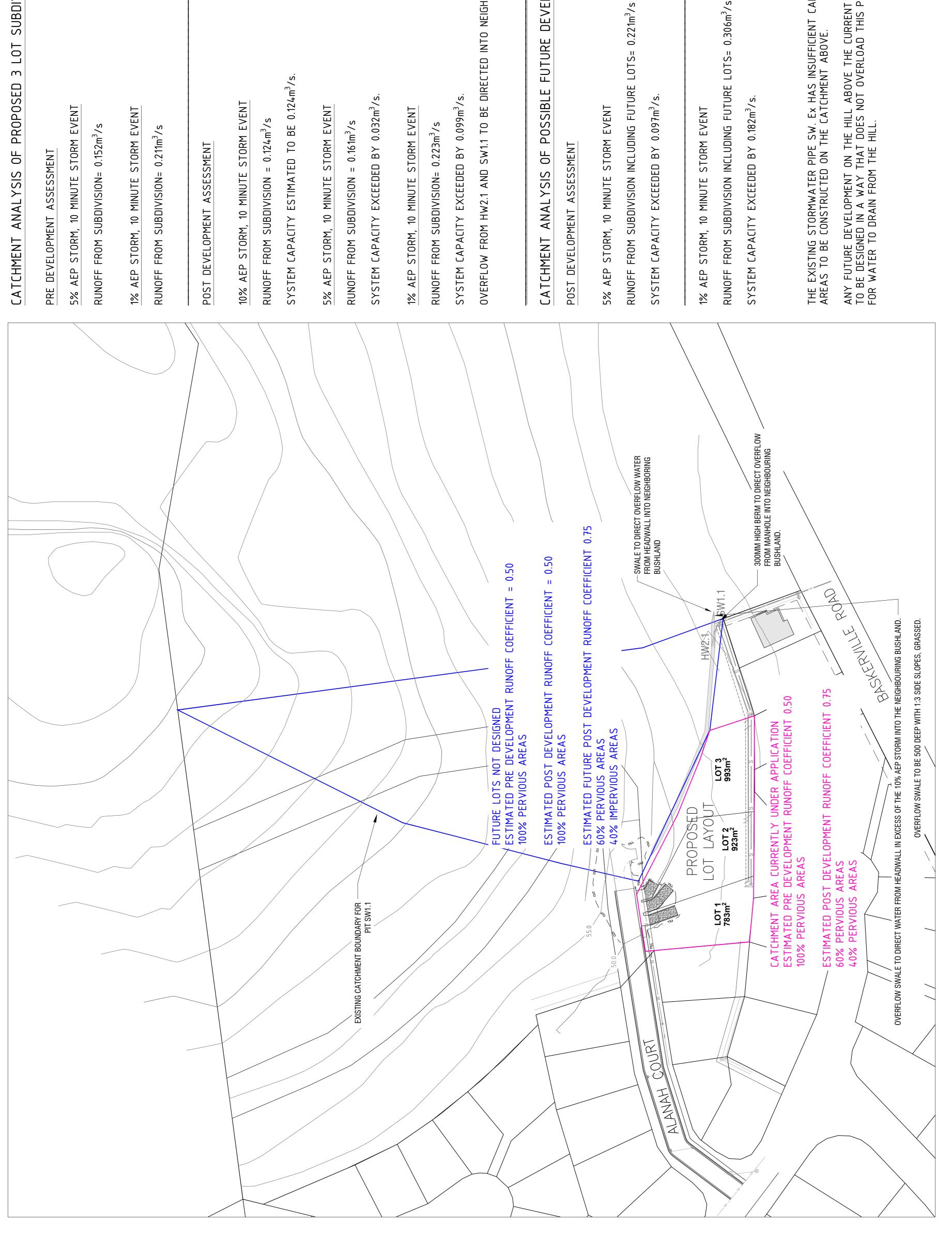
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. ACOF MI Dt.: 1th	CLIENT: ASCFIVII PLY LLO	Integral Consulting Engineers	Civil & Structural & Project Management			e: team@integralengineers.com.au w: www.integralengineers.com.au	
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SUBDIVISION. 3 LOT PROPOSED 9

PRE DEVELOPMENT ASSESSMENT

STORM, 10 MINUTE STORM EVENT

RUNOFF FROM SUBDIVISION= 0.152m<sup>3</sup>/s

10% AEP STORM, 10 MINUTE STORM EVENT

1% AEP STORM, 10 MINUTE STORM EVENT

RUNOFF FROM SUBDIVISION= 0.223m<sup>3</sup>/s

OVERFLOW FROM HW2.1 AND SW1.1 TO BE DIRECTED INTO NEIGHBOURING BUSHLAND.

POSSIBLE FUTURE DEVELOPMENT Ю

STORM, 10 MINUTE STORM EVENT

SYSTEM CAPACITY EXCEEDED BY 0.097m<sup>3</sup>/s.

1% AEP STORM, 10 MINUTE STORM EVENT

THE EXISTING STORMWATER PIPE SW. Ex HAS INSUFFICIENT CAPACITY FOR ADDITIONAL HARDSTAND AREAS TO BE CONSTRUCTED ON THE CATCHMENT ABOVE.

ANY FUTURE DEVELOPMENT ON THE HILL ABOVE THE CURRENT PROPOSED DEVELOPMENT WILL NEED TO BE DESIGNED IN A WAY THAT DOES NOT OVERLOAD THIS PIPE, AND PROVIDES A SAFE MEANS FOR WATER TO DRAIN FROM THE HILL.

DATE 3 LOT SUBDIVISION	20/11/2023 10 ALANAH CT. OLD BFACH	14/03/2024	22/04/2024   STORMWATER CATCHMENT & RUNOFF PLAN- 3 LOT SUBDIVISION	21/05/2024 1:7EA 1:7EA DRAWING No		DRAWN E.LEGG	DATE SEP 2023   C   C   C   C   C   C   C   C   C
No. AMENDMENT DESCRIPTION	A   FOR PLANNING APPROVAL	B FOR PLANNING APPROVAL	C CHANGES TO CATCHMENT DETAILS	D CHANGES TO CATCHMENT DETAILS			
			APPROVED:	10	3	Stephen Cole, Principal Engineer	D Eng (CVVII & ENVIOUMBEND), O'FENG WST Accreditation: Engineer Civil CC5900 T
	CLIENT. ASUF IMI PLY LLA		Integral Consulting Engineers	Civil ∞ Structural ∞ Project Management	m: 0417 650 474	e: team@integralengineers.com.au	w. www.integrateriginers.com.au a: Unit 10, 11 Morrison St, Hobart, 7000
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### INTEGRAL CONSULTING ENGINEERS

e: team@integralengineers.com.au w: www.integralengineers.com.au

a: Suite 21, 11 Morrison St, Hobart 7000 ABN: 23 627 152 041 **Civil** ∞ Structural ∞ Project Management

### STORMWATER ASSESSMENT

FOR A PROPOSED 3 LOT SUBDIVISION AT

10 ALANAH COURT, OLD BEACH

I.C.E. Project No: 22190

Client name: ASCF MI Pty Ltd

Document No. 22190-01 (Rev A)

11/06/2024

Document Approved by:

Stephen Cole BEng (Civil & Environmental) CPEng

Principal Civil / Structural Engineer Integral Consulting Engineers Pty Ltd WST Accreditation: Engineer Civil CC5900 T

### 1. Introduction

This stormwater management report presents a hydrological analysis of the proposed stormwater infrastructure for the 10 Alanah Court Subdivision in Old Beach. It evaluates the effects of post-development conditions on stormwater runoff. The assessment calculations were done using Autodesk's Civil 3D software, using rainfall data imported from the Bureau of Meteorology.

Appendix 1 contains the stormwater assessment results, and Appendix B shows the data behind the calculations.

### 2. Existing Site Conditions

The proposed development consists of one property, 10 Alanah Court, Old Beach. The total area of this property is 3.24Ha. The stormwater catchment area that drains to the stormwater system for this development is 1.45Ha and is contained entirely within the property.

The existing site is covered by predominantly scrubby bushland. One corner of the property was previously used as a quarry and is currently under rehabilitation.

The Aspect is southerly. Slope varies from flat at the top of the hill, to 25% towards the proposed lots.

The average annual rainfall is approx. 495mm (source: BOM Hobart Airport station, 10km away from the site).

The underlying geology is Jurassic Dolerite.

### 3. Stormwater Runoff and Drainage Assessment for the Proposed Development

### **Drainage System Overview**

The area of the proposed development of 3 lots and the associated road extension is 0.27 Ha, 19% of the catchment. The remainder of the catchment will remain unchanged.

Currently, runoff from the subject property flows onto the properties below as a sheet flow.

The proposed stormwater drainage system for the development consists of a stormwater cut-off drain above the 3 lots and a piped stormwater connection for each lot. The cut-off drain and pipe are proposed to be connected to the top end of an existing DN300 stormwater main that flows down to Baskerville Rd.

### **Minor Stormwater Event**

The minor stormwater event, the 5% Annual Exceedance Probability (AEP) flow, has been analysed.

Since most of the catchment will remain unchanged, the increase in flow due to the development is small. The main issue however is that flows from the catchment will be concentrated into the top of the existing stormwater pipe, SW1.1 on the design drawings.

The calculated flow into SW1.1 for the 5% AEP event is 0.156m3/sec. The calculated capacity of the existing stormwater pipe downstream from here is 0.124m3/sec. Therefore the existing pipe is unable to contain all of the 5% AEP flow from the development.

The estimated flow in the catchment prior to the development is 0.152m3/sec. This is also greater than the estimated capacity of the existing pipe.

A calculation has been done to determine what higher-frequency, lower-intensity rainfall event will be contained entirely within the pipe. This calculation found that the 20% AEP event will be contained within the pipe. This rainfall event is shown in the hydraulic grade line analysis on the stormwater pipe long section.

All higher intensity events will result in some surcharge from the stormwater manhole SW1.1. The design includes a 300mm high berm on the low side of the manhole to direct the overflow water into the bushland on the neighbouring property, 89 Baskerville Rd, Old Beach.

For larger storm events and if the inlet pipe blocks, headwall HW2.1 will overflow. The design includes a swale to direct the overflow water into the neighbouring bushland.

The owner of 89 Baskerville Rd, Old Beach has been notified about this development.

### **Major Stormwater Event**

The minor stormwater event, the 5% Annual Exceedance Probability (AEP) flow, has also been analysed.

The finction of the stormwater system for the the major event will operate in a similar way to the minor event, where some of the stormwater will be contained within the stormwater main, and part of it will surcharge from manhole SW1.1 and / or headwall HW2.1. The difference is that the amount of surcharge or overflow will be higher.

The berm on the low side of the manhole and the overflow channel from the headwall have been designed to contain all of the surcharge flow for the major stormwater event, and direct it into the neighbouring bushland.

### Management of the Existing Stormwater Main

As previously stated, the existing DN300 stormwater in 31 Baskerville Rd has insufficient capacity to contain all of the minor stormwater flow from the development and the upstream catchment.

A subdivision is planned for the land above the current proposed development. When that subdivision is implemented, additional stormwater capacity will be needed to drain that area down to Baskerville Rd or Alanah Court. To achieve an optimal drainage system for that subdivision, it is recommended that the design for that additional sotmrwater capacity be done for that future subdivision, and not as part of the current proposal.

Therefore this design allows for utilising the existing DN300 stormwater main and provision for overflow, and no additional drainage infrastructure below SW1.1.

### 4. Stormwater Quality Control

My opinion is that stormwater treatment infrastructure for this development would be impractical for Council to maintain.

Therefore I propose that Stormwater quality treatment is offset via a cost contribution from the developer to the Council, in accordance with the Brighton Council Stormwater Quality Control Contributions Policy.

### 5. Stormwater Quantity Control

We have been advised by the Council that the downstream stormwater network is at capacity.

The proposed development will result in a small increase in flows, 9L/s for the minor storm event and 12L/s for the major storm event.

A stormwater detention system on this slope for the small number of blocks is impractical to construct and maintain.

Therefore to ensure the development does not increase stormwater flows, I propose that the developer make a cost contribution to the Council for a larger stormwater detention system downstream. This contribution should be calculated proportionate to the additional flow created by the development relative to the total detention volume and the construction cost of the additional detention capacity.

6. Conclusion

This report and the associated calculations demonstrates that the subdivision design drawings

sufficiently address all of the stormwater management requirements, with the following exceptions:

stormwater quality - it is proposed that the developer make a cost contribution towards larger

infrastructure for these things in a more practical location.

stormwater detention -it is proposed that the developer make a cost contribution towards larger

infrastructure for these things in a more practical location.

The existing stormwater main downstream from the development has insufficient capacity for the 1% and 5% AEP flows. The system has been designed so that overflows from this stormwater system will be directed into 89 Baskerville Rd. The owner of the property has been notified. It is recommended

that additional stormwater capacity be designed as part of the proposed future development of the

catchment above.

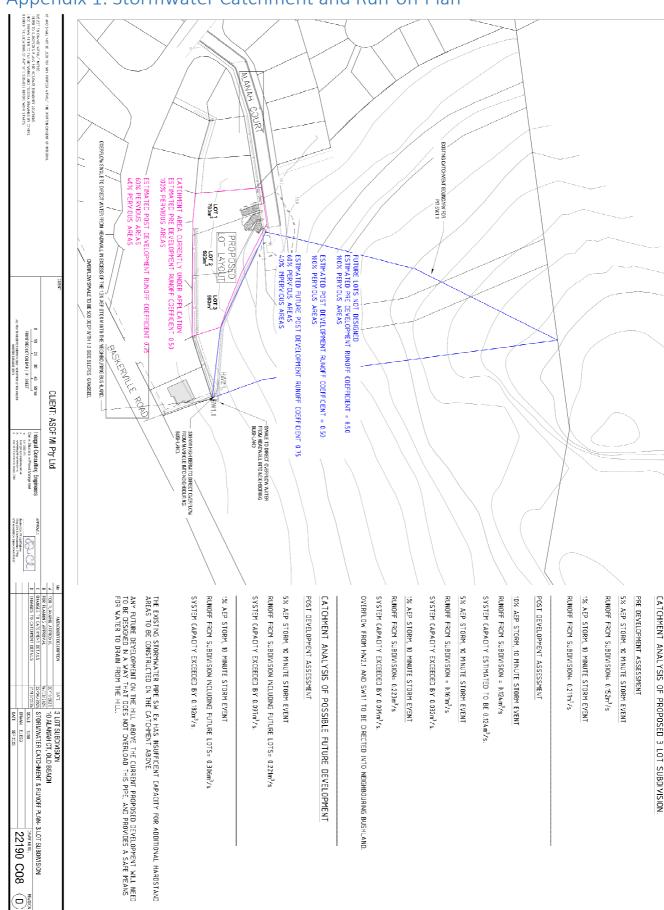
7. Appendices

Appendix 1: Stormwater Catchment and Run-off Plan

Appendix 2: Detailed Stormwater Calculations

Appendix 3: Photos

### Appendix 1: Stormwater Catchment and Run-off Plan



### Appendix 2: Detailed Stormwater Calculations

### Pre Development Assessment – 5% AEP

SW1.1	SW1.2	SW1.4		Name	SW1.4	SW1.2	SW1.1	Ex 1		Struct. ID	SW1.4	SW1.2	SW1.1	Ε <sub>χ</sub> 1		Struct. ID	SW1.2 - SV SW1.4	SW1.1 - SV SW1.2	SW Ex - SV SW1.1		Pipe
101.03	64.7	0.184	(m)	Stat.	0.005	0.004	0		(m)	Exit Ho	0.225	0.3	0.3		(m)	0	SV SW1.4	SV SW1.2	W SW1.1		From
11834.87	996.16	1709.69	(sq. m)	Drain. Are	0	0	0		(m)	ૂ	0.019	0.03	0.152		(cu. m/se (m)	O	SW1.2	SW1.1	Ex 1		То
0.5	0.5	0.5		Runoff Co	0	0	0		(m)	픙	64.532	36.425	33.603		(m)	_	64.532	36.425	33.603	(m)	3D Length
7.8	5.94	6	(min)	Time of Co	0	0	0		(m)	공	1.449	2.449	5.968		(m/s)	<	1709.69	996.16	33.603 11834.87 14540.72	(sq. m) (sq. m)	Drainage.
75.317	81.421	81.224	(mm/hr)	Rainfall Ir	0	0	0		(m)	He	0.083	0.068	0.117		(m)	a	1709.69	2705.85	14540.72	(sq. m)	Drainage,
0.124	0.011	0.019	(mm/hr) (cu.m/sec (cu.m/sec	Q=CIA/Kc	0	0	0		(m)	工	0.115	0.132	0.283		(m)	dc	0.5	0.5	0.5		Runoff Co
0	0	0	(cu. m/sec	Known Q	0	0	0		(m)	Total	0.107	0.306	1.817		(m)	v^2/2g	854.84	498.08	5917.44	(sq. m)	Area X "C"
<u></u>	<u>,</u>	<u>ئ</u>		Longitudir	0.19	0.374	1.934		(m)	皿	39.766	38.629	30.784	0	(m)	EGLo	854.84	1352.92	7270.36	(sq. m)	Area X "C"
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ь		<u>ы</u>	(m)	Gutter Wic Spread T	7.97	1.142	4.126			<del>-</del>	0.19	0.374	1.934		(m)	Ea	0.019	0.03	0.152	(mm/hr) (cu. m/set (cu. m/set (cu. m/set (m)	otal Q F
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0.103 (	0.564 (	0.378 (		W/T I	0.19	0.374	1.934		(m)	Ea	:	39.707	37.042	29.15	(m)	J/STOC	0.067	0.261	0.474	cu. m/ser (	ull Q
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_	1	ь	(m)	irate Leng C													1.449	2.449	5.968	m/s) (	elocity D S
1	1	1	(m)	Frate Wid (							N/A	N/A	Case A I			Step7*	0.742	0.248	0.094	(cu. m/se (m/s) (m/s) (min) (m)	èc Time I
			(m)	ົນrb Oper (							Case D	Case D	N/A			Step14*	40.898	39.387	36.692		nvert Elev I
1	-	!	(m)	Inlet Type Grate Leng Grate Wid Ourb Oper Ourb Oper Intercept F Bypass Flo													39.482 N/A	36.742 N/A	28.85 N/A	(m)	Pipe Dia. Full Q Velocity Fl Velocity D Sec Time Invert Elev Invert Elev Crown Drc Slope
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0	0	0	cu. m/sec	ypass Flc													2.20%	7.28%	24.00%		lope

### Pre Development Assessment – 1% AEP

SW1.1	SW1.2	SW1.4		Name		SW1.4	SW1.2	SW1.1	Ex 1		Struct. ID	SW1.4	SW1.2	SW1.1	Ex 1		Struct. ID	SW1.2 - SV SW1.4	SW1.1-SVSW1.2	SW Ex - SV SW1.1		Pipe
101.03	64.7	0.184	(m)	Stat.		0.009	0.007	0		(m)	Exit Ho	0.225	0.3	0.3		(m)	D					From
11834.87	996.16	1709.69	(sq. m)	Area A	Drain.	0	0	0		(m)	∓	0.027	0.041	0.211		(cu. m/se (m)	O	SW1.2	SW1.1	EX 1		То
0.5	0.5	0.5		Coeff. C	Runoff	0	0	0		(m)	픙	64.532	36.425	33.603		(m)	_	64.532	36.425	33.603	(m)	3D Length Drainage Drainage , Runoff Co. Area X "C" Area X "C" Time of Cc Time of Cc Rain "I" Runoff "Q' Known Q Total Q
7.8	5.94	0	(min)	Conc.	Time of F	0	0	0		(m)	동	1.579	2.69	6.505		(m/s)	<	1709.69	996.16	33.603 11834.87 14540.72	(sq. m) (	Drainage . [
104.239	112.053	111.801	mm/hr) (	Intens. Q	Rainfall	0	0	0		(m)	He	0.099	0.08	0.14		(m)	О	1709.69	2705.85	14540.72	(sq. m)	Drainage , R
0.171	0.016	0.027	(mm/hr) (cu. m/sec (cu. m/sec)	Q=CIA/Kc Known Q SL		0	0	0		(m)	Ŧ	0.136	0.156	0.295		(m)	dc v	0.5	0.5	0.5	s)	unoff Co. A
0	0	0	u. m/sec)	nown Q SL	nа	0	0	0		(m) (m)	Total Ei	0.127	0.369	2.158		(m) (m)	v^2/2g E0	854.84	498.08	5917.44	sq. m) (so	ea X "C" Ar
<b>4</b>	<u>,</u>	<u>,</u>		Slo	Longitudi nal Slope   Cross	0.226	0.449	2.298		(m)	<b>y</b> +	39.845	38.997	31.148	0	(m)	EGLo HO	854.84	1352.92	7270.36	(sq. m) (min)	ea X "C" Tin
0.02	0.02	0.02		Š	ss Cross	0.099	0.08	0.14		_	y+(P/gam DI	39.823	38.98	28.99	0	_	HGLo Sf	6	5.94	7.8	in) (min)	ne of Cc Tim
0.05	0.05	0.05	(cu.	Slope Sw Flow	ss Bypass	0.45	0.338	1.737		(m)	Eai	0.003	0.002	0		(m)	Tot	6 1:	6.681 10	7.8 10		e of Cc Rain
0	0	0	cu. m/se (cu. m/se (m)	v Flow	. Total ass Gutter	0.211	0.232	0.905			8	0 4	0 3	0		(m)	Total Pipe EGLi	111.801	108.939	104.239	(mm/hr) (cu. m/se(cu. m/se(cu. m/se(m)	ו"ו" Runo
0.171	0.016	0.027	m/ser(m)	Depth d	e -	0	0	0			C-theta	41.124 4	39.836	38.99 3		(m)	HGLi	0.027	0.041	0.211	m/ser(cu.ı	off "Q' Knov
0	0	0	(m)	n d Width	Gutter	0	0.47 1	0.609			eta Q	40.997 (	39.467 (	36.832		(m)	Ea	0 0	0	0	n/se (cu. r	n Q Total
ь	ш	ш	(m)			7.79	1.087	3.187		(m)	Ha	0.226 41	0.449 39	2.298 3		(m)	EGLa	0.027 0	0.041	0.211	n/ser(m)	
7 0.	1 0.	2		Spread T W/T		0 0.	0 0.	0 2		(m)	Ea	41.124	39.836 39.	38.99 37.	20	(m)	U/ST	0.225 0.	0.3 0.	0.3 0.	(cu. m	Dia. Full Q
0.082 Grate inlet	0.444 Grate inlet	0.3 Grate inlet				0.226	0.449	2.298				42.	39.707 40.	37.042 38.	29.15 30.001	(m)	OC Surfa	0.067 1.675	0.261 3.0	474 6.	cu. m/se( (m/s) (m/s) (min)	Velocit
nlei	nle	nlei	(m)	Inlet Type Length	Grate							42.862 Case B	40.504 Case B	38.772 N/A	001		ce E Step4*	375 1.579	3.695 2.	709 6.5	(m/s)	y Fı Velocit
Н	1	ш	(m)	Width	Grate							N/A	N/A	Case A			J/STOC Surface E Step4* Step7*	79 0.681	2.69 0.226	05 0.086	(min)	D Sec Tim
1-	1	1	(m)	Length	Ourb							Case D	Case D	N/A			Step14*	81 40.898	26 39.387	86 36.692	(m)	e Invert Ele
1	!	:	(m)	Height	Ourb Opening													39.482 N/A	36.742 N/A	28.85 N/A		ev Invert Ele
0.211	0.041	0.027	(cu. m/se	Length Height Flow Qi Flow Qb Structur	Intercept													2 N/A	2 N/A	5 N/A	(m)	Pipe Dia. Full Q Velocity Fi Velocity D Sec Time Invert Elev Invert Elev Crown Drc Slope
			(cu. m/sec (cu. m/sec)	Flow Qi Flow Qb Structure	Bypass													2.20%	7.28%	24.00%		Slope
0	0	0	0	Structure	Bypass																	

### Post Development Assessment – 10% AEP

				No.									#Line	VUKBAN	j						#Line						#010
3 HW2 1	2 SW1.2	1 SW1.3		Name			4 HW2.1	3 SW1.3	2 SW1.2	1 SW1.1	0 Ex 1		Struct. ID	DRAINAG	4 HW2.1	3 SW1.3	2 SW1.2	1 SW1.1	0 Ex 1		Struct. ID	4 sw2.1	3 SW1.2 - SV SW1.3	2 SW1.1 - SV SW1.2	1 SW Ex - SV SW1.1		- Ipc
00 7/0	64.7	0.184	(m)	Stat.			0.033	0.008	0.006			(m)	D Exit Ho	"URBAN DRAINAGE DESIGN MANUAL - Hydraulic engineering Circular No.22 inird Edition	0.3	0.225	0.3	0.3		(m)	D	HW2.1	SV SW1.3	SV SW1.2	SV SW1.1		
100000	7 996.16	4 1709.69	(sq. m)	Area A	Drain.		3 0.025	0	0	0		(m)	<b></b>	NUAL - Hy	3 0.09		3 0.038	3 0.124		(cu. m/se (m)	Q	SW1.1	SW1.2	SW1.1	굣1		ē
2	0.75	0.75		Coeff. C	Runoff		0	0	0	0		(m)	픙	raulic Eng	2.8/8		36.39	33.735		(m)	г	2.878	64.546	36.39	33.735	(m)	
>	5.94	6	(min)	Conc.	Time of		0	0	0	0		(m)	天	neering Cir	1.2.1	1.735	2.423	5.781		(m/s)	<	10682.8	1709.69	996.16	0	(sq. m)	0
200	69.298	69.126	(mm/hr)	Intens.	Rainfall		0	0	0	0		(m)	He	cutar No.2	0.3 1178	0.087	0.082	0.103		(m)	d	10682.8	1709.69	2705.85	13388.64	(sq.m)	0
8	0.014	0.025	(cu. m/set (cu. m/sec)	Q=CIA/Kc Known Q SL			0	0	0	0		_	Ξ.	2 Inira Ear	n/a	0.131	0.15	0.267		(m)	dc	0.5	0.75	0.75	0		
>	0	0	(cu. m/sec	Known Q S		1	0.025	0	0	0		(m)	Total	uon	0.082	0.154	0.299	1.705		(m)	v^2/2g	5341.4	1282.26	747.12	0	(sq. m) (	
	0.02	0.02			Longitudi nal Slope Cross	!	1.045	0.241	0.381	1.808		(m)			39.081	39.776	39.054	30.658	0	(m)	EGLo	5341.4	1282.26	2029.39	7370.78	(sq. m) (sq. m) (min)	
8	0.02	0.02		Slope Sx S			0.963	0.087	0.082	0.103		(m)	y+(P/gam DI		38.998	39.757	39.039	28.953	0	(m)	HGL0	9	6	5.94	0		
2	0.05	0.05	-	Slope Sw Flow	Cross B	:	0.741	0.417	0.313	1.022					0.009	0.003	0.002	0			Sť	9	6	6.62	9.009	(min) (mm/hr) (cu. m/se( cu. m/se( cu. m/se( (m)	
>	0.003	0	(cu. m/set (cu. m/set (m)		Prev. T Bypass G		1.062	0.2	0.221	0.487		(m)	Eai		0.025	0	0	0		(m)	Total Pipe EGLi	60.554	69.126	67.355	60.528	mm/hr) (o	
9	0.017	0.025	cu. m/ser (ı	Flow	Total Gutter		0	0	0	-0.822			CB C		SULUS	41.658	39.768	39.048		(m)		0.09	0.025	0.038	0.124	cu. m/sec (c	
>	0	0		Depth d Width	G		0	0	0.47	2.445			C-theta Op		39.023	41.504	39.469	37.343		(m)	HGLi Ea	0	0	0	0	cu. m/ser (c	
	ь	Ь	(m) (m)		Gutter		0	5.528	1.101	0			р На		7.00Z	0.241	0.381	1.808		(m) (r		0.09	0.025	0.038	0.124	u. m/se (n	
	ь	Ь	2	Spread T W/T			0	0	0	0		(m) (r	a Ea		39.122		39.768	39.048		(m)	EGLa U.	0.3	0.225	0.3	0.3	-	
2010 1010	0.519 Combinat	0.425 Grate inle					1.062	0.241	0.381	1.808		(m)	ш		ľ	ľ	39.707	37.59	29.15	(m)	/STOC S	0.487	0.078	0.233	0.491	u. m/sec (m	
	mbinat	ate inte	(m)	InletType Length	Gr										38.383 Case b	42.862 Case B	40.504 Case B	38.841 N/A	30.001	(m)	VSTOC Surface E Step4* Step7* Step14*	6.892	1.958	3.29	6.939	cu. m/se( (m/s) (m/s) (min) (m)	
	ᆸ	Ь	(m)		Grate Gr										ase b N/A						ep4* St	5.255	1.735	2.423	5.781	n) (s/r	
	ᆫ	1	1) (m)	Width Ler	Grate Op													Ä			ep7* St	0.009	0.62	0.25	0.097	nin) (m.	
	ᆫ		(m)	Length He	Curb Curb Opening Open										Case A	Case D	Case D	N/A			ep14*	38.06	41.418	39.387	37.24	1) (m)	
	0			Height Flo	Curb Curb Opening Opening Intercept Bypass																	37.354 N/A	39.482 N/A	37.29 N/A	28.85 N/A	n) (m)	
3	0.017	0.022	(cu. m/set (cu. m/sec)	w Qi Flo	ercept Byp										+												
>	0.001 SW1.1	0.003 SW1.2	ı. m/sec)	Flow Qi Flow Qb Structure	pass Bypass										+							25.33%	3.00%	5.77%	25.68%		
	/1.1	/1.2		ucture	pass																						

### Post Development Assessment – 5% AEP

				No.		İ							#Line	*URBA							#Line						#Line
3 HW2.1	2 SW1.2	1 SW1.3		Name			4 HW2.1	3 SW1.3	2 SW1.2	1 SW1.1	0 Ex 1		Struct. ID	N DRAINAC	4 HW2.1	3 SW1.3	2 SW1.2	1 SW1.1	0 Ex 1		Struct. ID	4 sw2.1	3 SW1.2	2 SW1.1	1 SW Ex -		Pipe
98.748	φ	0.184	(m)	Stat.			0.058	0.011	0.008			(m)	ID ExitHo	E DESIGN I		0.225				(m)	D	HW2.1	3 SW1.2 - SV SW1.3	2 SW1.1 - SV SW1.2	1 SW Ex - SV SW1.1		From
48 11594.29	64.7 996.16	84 1709.69	(sq. m)	Area A	Drain.		58 0.044	11	08	0		(m)	¥	1ANUAL - H	0.3 0.119	25 0.029	0.3 0.045	0.3 0.161		(cu. m/se (m)	0	SW1.1	SW1.2	SW1.1	区1		To
29 0.5	16 0.75	69 0.75		Coeff. C	Runoff		4	0	0	0		(m)	픙	ydraulic Er	19 2.878		45 36.39	51 33.735		se (m)	_	2.878	64.546	36.39	33.735	(m)	3D Lengt
.5 8.16	5.94		(min)	Onc.	Time of		0	0	0	0		(m)	H	*URBAN DRAINAGE DESIGN MANUAL - Hydraulic Engineering Circular No.22 Third Edition	8 1.689		9 2.538	6.213		(m/s)	<	<sup>78</sup> 11594.29	1709.69	996.16	0	(sq. m)	h Drainage
6 74.136	4 81.421	6 81.224	(mm/hr)	Intens.	Rainfall		0	0	0	0		(m)	He	Sircular No	0.3	0.	8 0.089	3 0.118		(m)	<u>a</u>	9 11594.29	9 1709.69	6 2705.85	0 14300.14	(sq. m)	Drainage
6 0.119	1 0.017	4 0.029		Q=CIA/Ko			0	0	0	0		(m)	工	.22 Third E	3 n/a	5 0.142	9 0.163	8 0.286		(m)	ਨ	9 0.5	9 0.75	5 0.75	0		. Runoff Co
0	0	0	(cu. m/sec (cu. m/sec)	Q=CIA/Kc Known Q SL			0.044	0	0	0		(m)	Total	dition	0.145	0.167	0.329	1.969		(m)	v^2/2g	5797.15	1282.26	747.12	0	(sq. m)	Area X "C
4	0.02	0.02	С	SI	nal Slope Cross	Longitudi	1.369	0.263	0.418	2.087		(m)	Ш		39.386	39.815	39.335	30.937	0	(m)	EGLo	5797.15	1282.26	2029.39	7826.53	(sq. m) (min)	'Area X "C"
0.02	0.02	0.02		SlopeSx			1.224	0.095	0.089	0.118		(m)	y+(P/gam DI		39.24	39.788	39.315	28.968	0	(m)	HGLo	8.16	6	5.94	0		3D Length Drainage . Drainage . Runoff Co   Area X "C" Area X "C" Time of C. Time of C. Rain "!" Runoff "Q' Known Q Total Q
0.05	0.05	0.05		Slope Sw Flow	Cross		0.985	0.49	0.369	1.329					0.015	0.004	0.002	0			Sf	8.16	6	6.594	8.168	(min)	Time of Cc
0 NA	0 N A	0 N A	cu. m/set (cu. m/set (m)		Bypass (	Prev. T	1.398	0.223	0.246	0.581		(m)	Eai		0.044	0	0	0		(m)	Total Pipe EGLi	74.136	81.224	79.276	74.108	(mm/hr) (cu. m/se(cu. m/se(cu. m/se(m)	ain "I"
			cu. m/ser (	Flow	Gutter	Total	0	0	0	-0.743			CB CB		39.429	41.68	39.805	39.327		(m)		0.119	0.029	0.045	0.161	cu. m/ser (	unoff "Q' k
NA NA	NA NA	NA NA		Depth d W	G		0	0	0.469	2.385			C-theta C		39.284	41.513	39.476	37.358		(m)	HQL:	0	0	0	0	cu. m/ser (	nown Q T
A NA	A NA	A NA	(m) (m)	Width Sp	Gutter		0	5.426	1.07	0		=	ę На		1.398	0.263	0.418	2.087		(m)	E .	0.119	0.029	0.045	0.161	ນ. m/seເ (n	
A NA	A NA	A NA	2	Spread T W/T			0	0	0	0		(m) (m)	a Ea		39.458	41.68	39.805	39.327		(m)	EGLa U.	0.3	0.225	0.3	0.3		Pipe Dia. Fu
							1.398	0.263	0.418	2.087		3			ľ	ľ	39.707	37.59	29.15	(m) (m)	U/STOC Surface E Step4*	0.487	0.078	0.233	0.491	(cu. m/se (m/s)	Full Q Ve
Grate inle NA	Combinat NA	Grate inte NA	(m)	Inlet Type Length	Grate										38.585 Case B	42.862 Case B	40.504 Case B	38.841 N/A	30.001	=	ırface E Ste	6.892	1.958	3.29	6.939		ocity Fi Vel
NA	N <sub>A</sub>		(m)	gth Width	ite Grate										se B N/A		se B N/A					5.693	1.812	2.538	6.213	(m/s) (mi	ocity D Sec
NA	NA					Curb												Case A N/A			Step7* Ste	0.008	0.594	0.239	0.09	(min) (m)	Time Inve
NA	NA		(m)	Length Height	ning Ope	b Qurb									Case A	Case D	Case D				Step14*	38.06 3	41.418 3	39.387	37.24	(m)	rt Elev Inve
	_	_	(cu. 1	ht Flow	ning Inter										-							37.354 N/A	39.482 N/A	37.29 N/A	28.85 N/A	(m)	Velocity Fi Velocity D Sec Time Invert Elev Invert Elev Crown Drc Slope
0.124 0	0.045	0.029	(cu. m/ser (cu. m/sec)	Qi Flow	cept Bypa:																	25.	ω	ĆΊ	25		m Drc Slope
0.037 OFFSITE	0 SW1.1	0 SW1.2	n/sec)	Flow Qi Flow Qb Structure	Opening Opening Intercept Bypass Bypass																	25.33%	3.00%	5.77%	25.68%		

### Post Development Assessment – 1% AEP

No. 1.   N		Pipe	From	To	3D Length	Drainage	, Drainage	3D Length Drainage, Drainage, Runoff Co. Area X "C"		Area X "C" Time of Cc Time of Cc Rain "I"	ime of CC III	ne of Cc Rain		off "Q" Knov	Runoff"Q' Known Q Total Q Pipe Dia. Full Q	Q Pip	ne Dia. Fu		elocity H V	elocity D So	ec Time In	vert Elev Inv	Velocity Fi Velocity D Sec Time Invert Elev Invert Elev Crown Drc Slope	n Drc Stope	
0 7205-55					(m)	(sd. m)	(sq. m)		(sq. m)					m/se (cu.	m/sec(cu. r	m/sec(m,		u. m/se <sub>(1</sub>							
1.2   2.023.3   5.94   6.547   10.95  0.04   0.062   0.062   0.075   0.076   0		SW Ex - S	W SW1.1	EX 1	33.735		14300.14			7826.53	0			0.223		0.223	0.3	0.491	6.939	6.771	0.083	37.24	28.85 N/A	25.	%89
8.2.5         1.282.5         6         1.11.801         0.044         0.255         0.025         1.958         1.958         0.547         41.418         33.482 N/A           9.1.5         5797.15         8.16         1.02.75         0.165         0.25         0.078         6.256         0.08         38.06         37.554 N/A           2.9.5         579.14         8.16         1.02.756         0.165         0.25         0.076         6.256         0.08         38.04         38.02         38.04         38.04         38.02         38.04         38.04         38.02         38.04		SW1.1 - S	3V SW1.2	SW1.1	36.39					2029.39	5.94			0.062		0.062	0.3	0.233	3.29	2.779	0.218	39.387	37.29 N/A	ις	%/_/
99.15         51.95         61.15         0.165         0.165         0.246         0.246         0.206         0.008         38.06         37.354 NIA           28.16         HGLO         ST.         Total Pipe GLI         HGLI         HGLI <t< td=""><td></td><td>3 SW1.2 - S</td><td>3V SW1.3</td><td>SW1.2</td><td>64.546</td><td></td><td></td><td></td><td></td><td>1282.26</td><td>9</td><td></td><td>1.801</td><td>0.04</td><td></td><td>0.04</td><td>0.225</td><td>0.078</td><td>1.958</td><td>1.968</td><td>0.547</td><td>41.418</td><td>39.482 N/A</td><td>8</td><td>%00</td></t<>		3 SW1.2 - S	3V SW1.3	SW1.2	64.546					1282.26	9		1.801	0.04		0.04	0.225	0.078	1.958	1.968	0.547	41.418	39.482 N/A	8	%00
Color   Colo		4 sw2.1	HW2.1	SW1.1	2.878	11594.26	11594.29			5797.15	8.16			0.165		0.165	0.3	0.487	6.892	6.226	0.008	38.06	37.354 N/A	25.	33%
(m)		Struct. IC	0	0	_	>	Б	gc	v^2/2g			Tota	al Pip∉ EGLi			EG	Т		Surface E S			ep14*			
2.338         3.1.331         28.962         0         39.721         37.582         2.481         39.721         37.59         38.841         NA         Case A         NA         NA         Case A         NA			(m)	(cn. m/s	e (m)	(m/s)	Œ)	(m	(E)		(m	(E)	Œ			E)			m)						
2.33         31.331         28.962         0.004         0.34721         37.382         2.481         37.59         38.841         N/A         Case A         N/A		区1								0								29.15	30.001						
0.039 39.736 38.689 0.004 0.148 39.885 38.946 0.515 39.902 39.707 40.504 Case B N/A Case A N/A N/A Case A Case A N/A Case A N/A Case A N/A Case A N/A Case A Case A N/A Case A Case A N/A Case A N/A Case A N/A Case A N/A Case A N/A Case A N/A Case A Case A N/A Case A Case A N/A Case A N/A Case A Case A N/A Case A N/A Case A N/A Case A Case A N	_ <	1 SW1.1	9.0							31.331	28.992	0					39.721	37.59	38.841 N						
0.256   0.04   64.546   1.968   0.114   0.167   0.197   39.822   39.831   0.006   0.147   0.147   39.817   0.004   0.147   39.817   0.004   0.147   39.817		2 SW1.2	9.0					l n/a	0.039		39.698	0.004					39.902	39.707	40.504 C			aseA			
0.279 38.833 38.553 0.029 0.084 39.917 38.637 1.913 38.973 38.585 Case B N/A Case A Case		3 SW1.3	0.225							39.922	39.871	0.008				0.312			42.862 C			aseD			
I   E   Y+(P/gam D  Eai	- 1	1 HW2.1	9.0					i n/a	0.279		39.553	0.029				1.913	39.973		38.585			aseA			
Struct ID         Exit Month         (m)	=	DRAINAGE	DESIGN MA	ANUAL - Hy	draulic Eng	ineering G	ircular No.	22 Third Ec	lition																
EN 1   Marie		Struct. IE	5 Exit Ho	÷	운	웃	롼	Ŧ	Total		'+(P/gam DI	Eai		St		Ε̈́Ξ		m							
Ex 1         Ex 1         Control (sq. m)         Control (sq. m) <th< td=""><td></td><td></td><td>(E)</td><td>(E)</td><td>(m)</td><td>(E)</td><td>(E</td><td>(m</td><td></td><td></td><td>m)</td><td>(E)</td><td></td><td></td><td></td><td>E</td><td></td><td>(H</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>			(E)	(E)	(m)	(E)	(E	(m			m)	(E)				E		(H							
SW11         0         0         0         0         2.481         0.426         0.426         0.056         0.056         0.057         0.057         0.055         0.055         0.057         0.057         0.055         0.057         0.057         0.055         0.057         0.058         0.058		) Ex 1																							
SW12         0.005         0.148         0         0.148         0.496         0.599         0.556         0.0467         0.751         0.009         0.518         0.013         0.014         0.009         0.148         0.025         0.0467         0.051         0.051         0.012         0.012         0.014         0.054         0.256         0.056         0.0467         0.058         0.058         0.054         0.056         0.056         0.058         0		1 SW1.1							0	2.481	0.142	1.842	1.018		2.382	0	0	2.481							
SW1.3         0.02         0         0         0         0.312         0.136         0         0.312         0.136         0         0.312         0         0         0.312         0         0.312         0         0.313         0         0         0.312         0         0.313         0         0         0.313         0         0         0.313         0			0.016								0.459	0.509	0.506			0.751	0.00	0.515							
HW21   Collid   Col		3 SW1.3	0.02						0	0.312	0.114	0.674	0.276	0		5.189	0	0.312							
Drain.   Runoff Time of Rainfall   Runoff Time of Runoff Time of Rainfall   Runoff Time of Rainfall   Runoff Time of Runoff Time of Rainfall   Runoff Time of Rainfall   Runoff Time of Rainfall   Runoff Time of Rainfall   Runoff Time of Runoff Time of Rainfall   Runoff Time of Runoff Tim			0.112							1.857	1.577	1.365	1.913	0	0	0	0	1.913							
Stat.         Area of Coeff. Conc.         Intensity of Conc.				Drain	Rinoff	Time of				Longitudi				_ 1	diff.	<u> </u>						ğ		Pyroas	
(m)         (min)         (min/hr)         (mi		Name	Stat.	Area A	Coeff. C	Conc.		Q=QAVKc		SL S	ŏ		,				ead T W		let Type Le			0	0	Qi Flow	2b Structure
0.184 1709.69 0.75 6 111.801 0.04 0 0.02 0.05 0.05 0 NA			(m)	(sq. m)		(min)	(mm/hr)	(cu. m/ser	(cu. m/sec	_		(cn.	m/sec (cu.	m/se <sub>i</sub> (m)	(m)	m)	_		ت					n/sec (cu. m	/sec)
64.7 996.16 0.75 5.94 112.053 0.023 0 0.02 0.05 0.08 0 NA NA NA NA Ombinat NA NA NA NA NA O.086105 0 NA		1 SW1.3	0.18							0.02	0.02	0.05	0 NA	NA	NA	NA			rate inle						008 SW1.2
98.748 11594.29 0.5 8.16 102.726 0.165 0 -1 0.02 0.05 0 NA NA NA NA NA Grate inter NA NA NA 0.165		2 SW1.2	64.7							0.02	0.02	0.05	0 NA	N	NA	NA			ombinat N						004 SW1.1
	٠.)	3 HW2.1	98.748	8 11594.2						Ļ	0.02	0.05	0 NA	NA	N	NA			rate inter N					.165	0

### Post Development Assessment, Assumed Development of Catchment Above — 5% AEP

HW2.1	SW1.2	SW1.3		Name			1.74411	L C/WH	SW1.3	SW1.2	SW1.1	Ex 1		Struct. ID	HW2.1	SW1.3	SW1.2	SW1.1	EX 1		Struct. ID	sw2.1	SW1.2 - SV SW1.3	SW1.1-SVSW1.2	SW Ex - SV SW1.1		Pipe
98.748	64.7	0.184	(m)	Stat			0.101	0 121	0.011	0.008	0		(m)	Exit Ho	0.3	0.225	0.3	0.3		(E	D	HW2.1	/SW1.3	/SW1.2	/SW1.1		From
11594.29	996.16	1709.69	(sq. m)	Area A	Drain.		0.000		0	0.078	0		(m)	∓	0.179	0.029	0.045	0.221		(cu. m/se (m)	Q	SW1.1	SW1.2	SW1.1	Ex 1		То
0.75	0.75	0.75		Coeff. C	Runoff		c	5	0	0	0		(m)	픙	2.878	64.546	36.39	33.735		<u>a</u>	_	2.878	64.546	36.39	33.735	(m)	3D Length
8.16	5.94	6	(min)	Conc.	Time of F		c	0	0	0	0		(m)	공	2.533	1.812	0.632	6.752		(m/s)	<	11594.29		996.16	0	(sq. m) (	Drainage [
74.136	81.421	81.224	(mm/hr) (	Intens. Q	Rainfall		c	0	0	0	0		(m)	He	0.3 n/a	0.095	0.3 n/a	0.141		(E)	О	11594.29	1709.69	2705.85	14300.14	(sq. m)	Drainage, R
0.179	0.017	0.029	(cu. m/sec (cu. m/sec)	Q=CIA/Kc Known Q SL			c	0	0	0	0		(m)	I.	1/a	0.142	ı/a	0.296		(m)	dc v	0.75	0.75	0.75	0		3D Length Drainage Drainage , Runoff Co. Area X "C" Area X "C" Time of Cc Time of Cc Rain "I"
0	0	0	u. m/sec)	nown Q SL	na	Б	0.000	0 000	0	0.078	0		(m)	Total Ei	0.327	0.167	0.02	2.325		(m)	v^2/2g ⊟	8695.72			0	S)	rea X "C" Ar
-1	0.02	0.02			nal Slope Cross	Longitudi		1 976	0.263	0.406	2.467		(m) (m)		39.838	39.813	39.715	31.317	0	(m)	EGLo H	8695.72	1282.26	2029.39	10725.1		ea X "C" Tir
0.02	0.02	0.02		Slope Sx Slo			<u>-</u>	1 5/10	0.095	0.385	0.141			y+(P/gam DI	39.51	39.786	39.694	28.991	0	(m)	HGLo Sf	8.16	0	5.94	0	(min) (m	ne of Ca Tir
0.05	0.05	0.05	(cı	Slope Sw Flow	Cross By	Prev.	1.4/	1 477	0.49	0.369	1.821		(m)	Eai	0.034	0.004	0.002	0		(m)	To	8.16		6.594	8.168	(min) (m	ne of Cc Ra
0 NA	0 NA	0 NA	cu. m/se (cu. m/se (m)	w Flow	Bypass Gutter	v. Total	1.014	1 0/15	0.223	0.41	0.995			8	0.099	0	0.078	0		(m)	Total Pipe EGLi	74.136	81.224	79.276	74.111	(mm/hr) (cu. m/sec (cu. m/sec (cu. m/sec (m)	in "I" Ru
NA	NA	NA	. m/set (m)		ter	al	c	0	0	0	-0.6			Ct.	39.936	41.68	39.792	39.707		) (m)	н нец	0.179	0.029	0.045	0.221	. m/ser (cu	າoff"Q'Kno
NA	NA	NA	(m)	Depth d Width	Gutter		c	0	0	0.469	2.286			C-theta Op	39.609	41.513	39.772	37.381		(m)	Li Ea	0	0	0	0	. m/ser (cu.	Runoff "Q' Known Q Total Q
NA	N <sub>A</sub>	NA A	(m)		ter		c	0	5.426	0.869	0		(m)	На	1.942 4	0.263	0.415	2.467		(m)	EGLa	0.179			0.221	.m/se(m)	al Q Pipe
NA	N A	NA		Spread T W/T			c		0	0.005	0		(m)	Ea	40.002	41.68	39.802	39.707		(m)		0.3			0.3	(cu.	Pipe Dia. Full Q
Grat	Com	Grat					1.042	1 0/10	0.263	0.415	2.467				w	4	39.707 4	37.59	29.15 3	(m)	TOC Sur	0.487				m/ser (m/s	
Grate in le NA	Combinat NA	Grate in let NA	(m	Inlet Type Length	Grate										38.585 Case B	42.862 Case B	40.504 Case B	38.841 N/A	30.001		face E Step	6.892				(m/s	city Fi Velo
NA	NA	N <sub>A</sub>	(m)	th Width	e Grate										B N/A	B N/A	e B N/A	Case A			U/STOC Surface E Step4* Step7* Step14*	6.36				3	city D Sec T
NA	NA	Ä	(m)	Length		Qurb									Case A	Case D	Case A	A/N/A			7* Step:	0.008	_			(m)	ime Inver
NA	NA	NA A	(m)	h Height	ing Open	Qurb									Þ	Ö	Þ				14*	38.06 37				3	Elev Invert
0.			(cu. m		ing Interc																	37.354 N/A	39.482 N/A	37.29 N/A	28.85 N/A	(m)	Velocity F. Velocity D Sec Time Invert Elev Invert Elev Grown Drc Slope
0.124 0.	0.45	0.25	(cu. m/sec (cu. m/sec)	Qi Flow	ept Bypas																	25.33%	3.0	5	25.		Drc Slope
0.097 OFFSITE	0 SW1.1	0 SW1.2	/sec)	Flow Qi Flow Qb Structure	Opening Opening Intercept Bypass Bypass																	33%	3.00%	5.77%	25.68%		

### Post Development Assessment, Assumed Development of Catchment Above $\,-\,1\%$ AEP

				No.							#Line	*URBA							#Line						# [
3 HW/3 1	2 SW1.2	1 SW1.3		Name	4 HW2.1	3 SW1.3	2 SW1.2	1 SW1.1	0 反1		Struct. ID	N DRAINAG	4 HW2.1	3 SW1.3	2 SW1.2	1 SW1.1	0 Ex 1		Struct. ID	4 sw2.1	3 SW1.2 -	2 SW1.1-	1 SW Ex -		- 100
00 740	64.7	0.184	(m)	Stat.	0.251	0.02	0.016			(m)	ID Exit Ho	*URBAN DRAINAGE DESIGN MANUAL- Hydraulic Engineering Circular No.22 Third Edition	0.3	0.225	0.3	0.3		(m)	D	HW2.1	SW1.2 - SV SW1.3	SW1.1 - SV SW1.2	SW Ex - SV SW1.1		-
1150100	7 996.16	4 1709.69	(sq. m)	Drain. Are	1 0.189	0	6 0.148	0		(m)	폭	ANUAL - Hyd	3 0.248	0.04	3 0.062	3 0.306		(cu. m/se (m)	Q	SW1.1	SW1.2	SW1.1	E <sub>X</sub> 1		
2	0.75	0.75		Runoff Co	0	0	0	0		(m)	퓽	draulic Engi	2.878	64.546	36.39	33.735		(m)	_	2.878	64.546	36.39	33.735	(m)	
	5.94	6	(min)	Time of Cc	0	0	0	0		(m)	공	neering Cir	3.51	1.968	0.873	7.313		(m/s)	<	11594.29	1709.69	996.16	0	(sq. m)	0
1	112.053	111.801	(mm/hr) (	Rainfall In	0	0	0	0		(m)	퓬	cular No.2:	0.3 n/a	0.114	0.3	0.172		(m)	۵	11594.29	1709.69	2705.85	14300.14	(sq. m)	c
,	0.023	0.04	(cu. m/sec (cu. m/sec)	Q=CIA/Kc K	0	0	0	0		(m)	<u>I</u>	2 Third Edit	n/a	0.167	n/a	0.299		(m)	dc	0.75	0.75	0.75	0		
•	0	0	cu. m/sec)	Drain. Are Runoff Co. Time of Cc. Rainfall In Q-CIA/Kc. Known Q. Longitudii Cross Slor Cross Slor Prev. Bypa Total Gutt Depth	0.189	0	0.148	0		(m)	Total Ei	ion	0.629	0.197	0.039	2.728		(m)	v^2/2g E	8695.72	1282.26	747.12	0	(sq. m) (s	
	0.02	0.02		ongitudir Cı	2.521	0.312	0.917	2.9		(m)			40.391	40.337	40.155	31.75	0	(m)	EGLo H	8695.72	1282.26	2029.39	10725.1	(sq. m) (n	
,	0.02	0.02		Oss Slot Q	1.892	0.114	0.878	0.172		(m)	y+(P/gam DI		39.763	40.286	40.116	29.022	0	(m)	HGLo Sf	8.16	6	5.94	0	(min) (m	
	0.05	0.05	(CI	oss Slop Pri	2.047	0.674	0.509	2.524		(m)	Eai		0.066	0.008	0.004	0		(m)		8.16	6	6.547	8. 167	(min) (m	
,	0 NA	0 NA	(cu. m/sec (cu. m/sec (m)	ev. Bypa Tot	2.646	0.276	0.925	1.911		=	B		0.189	0	0.148	0		n) (m)	Total Pipe EGLi	102.726	111.801	109.504	102.697	(mm/hr) (cu. m/se((cu. m/se((m)	
	NA	NA	. m/se(m)	al Gutt Dep	0	0	0	-0.6					40.581	41.729	40.304	40.14		) (m)	HGLI	0.248	0.04	0.062	0.306	. m/se (cu	
	¥	NA	(m)	۵	0	0	0.467	2.284			C-theta Op		39.952	41.532	40.265	37.412		(m)	Ea	0	0	0	0	. m/ser(cu.	
	Z	NA	(m)	Gutter Wic Spread T	0	5.189	0.237	0		(m)	Ha		2.646 4	0.312 4	0.93 4	2.9		(m)	EGLa	0.248	0.04	0.062	0.306	m/ser (m)	
	Z	NA		ad T W/T	0	0	0.005	0		(m)	Ea		40.706	41.729	40.317 3	40.14		(m)	_	0.3	0.225	0.3	0.3	(cu.	
)	Comb	Grate			2.646	0.312	0.93	2.9					32	42	39.707 40	37.59 38	29.15 30	(m)	J/STOC Surf	0.487 6	0.078 1	0.233	0.491 6	cu. m/set (m/s)	
	Combinat NA	Grate inle NA	(m)	Type Grate									38.585 Case B	42.862 CaseB	40.504 CaseB	38.841 N/A	30.001		Surface E Step4*	6.892 6.	1.958 1.	3.29 2.	6.939 7.	) (m/s)	
	¥	Ä	(m)	Leng Grate V									B N/A	B N/A	B N/A	Case A			1* Step7*	6.919 0.0	1.968 0.5	2.779 0.3	7.313 0.0	(min)	
:	NA	NA	(m)	Mid Ourb Op									Case A	Case D	Case A	A N/A			* Step14*	0.007 38.06	0.547 41.418	0.218 39.387	0.077 37.24	(m)	
	N A	NA	(m)	per Curb Ope															*	06 37.354 N/A	18 39.482 N/A			(m)	
	0.062	0.04	(cu. m/sec	ntercept F																4 N/A	2 N/A	37.29 N/A	28.85 N/A	(m)	
	0 SW1.1	0 SW1.2	(cu. m/sec (cu. m/sec)	Inlet Type Grate Lens Grate Wid Ourb Oper Ourb Oper Intercept i Bypass Flu Bypass St																25.33%	3.00%	5.77%	25.68%		

### Appendix 3: Photos



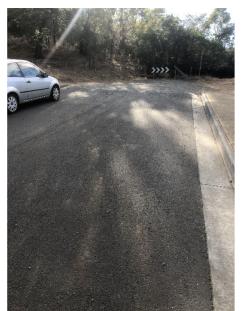


Photo 3: View of the site, from the end of the existing road.



Photo 4: View of the site including existing fire trail



Photo 5: view of the site including the rear of lots where the stormwater line will be constructed



### BUSHFIRE HAZARD REPORT 3 LOT SUBDIVISION & BALANCE 10 ALANAH COURT, OLD BEACH



CERTIFIED BY N M CREESE

21st December 2023

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### CONTENTS

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ATTACHMENT 1 - SUBDIVISION PLAN		

ATTACHMENT 2 - BUSHFIRE HAZARD MANAGEMENT PLAN

ATTACHMENT 3 - PLANNING CERTIFICATE

AS 3959:2018 cannot guarantee that a habitable building will survive a bushfire attack, however the implementation of the measures contained within AS 3959:2018, this report and accompanying plan will improve the likelihood of survival of the structure. This report and accompanying plan are based on the conditions prevailing at the time of assessment. No responsibility can be accepted to actions by the landowner, governmental or other agencies or other persons that compromise the effectiveness of this plan. The contents of this plan are based on the requirements of the legislation prevailing at the time of report.



### 1. SUMMARY:

This Bushfire Hazard Report has been prepared to support the development of a new 3 lot and balance residential subdivision at 10 Alanah Court, Old Beach. The site is subject to a bushfire prone areas overlay under the under the relevant planning scheme and has also been deemed to be bushfire prone due to its proximity to the areas of bushfire prone vegetation surrounding the site.

This report identifies the protective features and controls that must be incorporated into the design and construction works to ensure compliance with the standards. Fire management solutions are as defined in AS 3959:2018 Construction of Buildings in Bushfire-Prone Areas and C13.0 Bushfire Prone Areas Code, Tasmanian Planning Scheme - Brighton (Code).

All lots have been designed to achieve a bushfire attack level of BAL-19 (or lower) of AS 3959:2018 in accordance with C13.0 the Code. New habitable buildings on these lots are to be constructed to this level, or greater, with the establishment and maintenance of the specified Hazard Management Areas to ensure ongoing protection from the risk from bushfire attack. A reduced bushfire attack level may be permitted where the separation distance between the bushfire prone vegetation and the building exceeds that required for BAL-19, subject to a revised assessment at the time of application for building approval.

Compliance with the following provisions of the *Code* will be required:

- C13.6.1 Provision of hazard management areas
- C13.6.2 Public and fire fighting access
- C13.6.3 Provision of water supply for fire fighting purposes

The effectiveness of the measures and recommendations detailed in this report and AS 3959:2018 is dependent on their implementation and maintenance for the life of the development or until the site characteristics that this assessment has been measured from alter from those identified. No liability can be accepted for actions by lot owners, Council or governmental agencies which compromise the effectiveness of this report.

This report has been prepared and certified by Nick Creese, principal of Lark & Creese Surveyors. Nick is a registered surveyor in Tasmania and is accredited by the Tasmanian Fire Service to prepare Bushfire Hazard Management Plans (scope 1, 2, 3a, 3b & 3c.

Site survey was carried out on 24th November 2022.



### 2. LOCATION:

Property address: 10 Alanah Court, Old Beach

Title owner: Thinking of Marketing Pty Ltd

Title reference: C.T. 184468/11

PID N°: 2270100

Title area: 3.241 Ha

Municipal area: Brighton

Zoning: General Residential/Rural

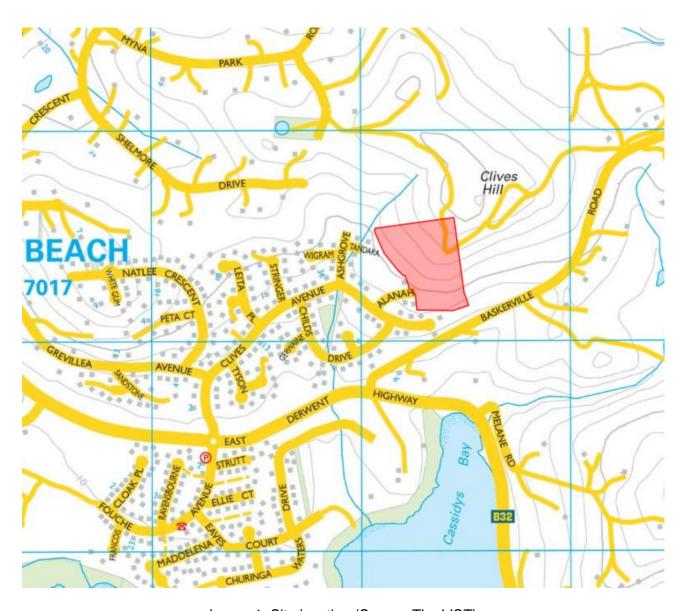


Image 1: Site location (Source The LIST)

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### 3. SITE DESCRIPTION:

The site is located at the end of Alanah Court, approximately 600m north east of the intersection of Clives Avenue and East Derwent Highway, Old Beach. The site is located at an elevation range of approximately 40-100 metres, with grades typically falling to the south and south west in the order of 10-15°.

At the time of assessment the site was undeveloped and was vegetated by a mix of grassed areas in the east and areas of native trees and shrubs in the north and south. At the northeast corner of the site was part of a disused quarry.

The allotments to the north and east consisted of a disused quarry and areas of native trees and shrubs.

To the south and west of the site was a well-established area of residential allotments, Baskerville Road, Alanah Court, Clives Avenue, Shelmore Drive, and Tandara Court. The residential allotments included dwellings, sheds, accesses, and gardens. The roads included grassed nature strips, concrete footpaths, and bitumen carriageways. A new residential subdivision has just been completed to the west of the site and included bitumen roads and vacant lots. Minimal vegetation existed across the lots.

Reticulated water supply is available to the site with domestic water supply requirements reliant on TasWater mains supply.





Image 2: Aerial image of site and surrounds (Source: The LIST)





Image 3: Looking south east towards development site.

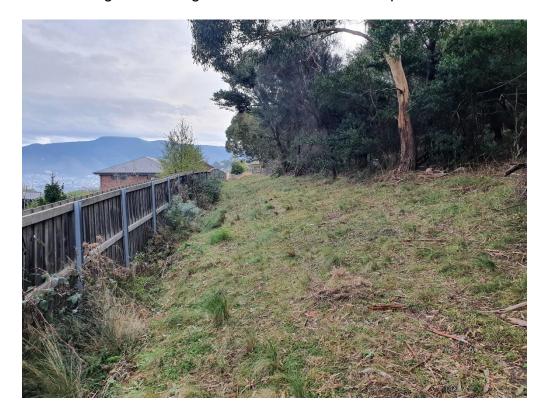


Image 4: Looking west towards development site.

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## **Planning Controls:**

Planning controls are administered by the Brighton Council under the *Tasmanian Planning Scheme - Brighton*. The site is subject to the Natural Assets Code and Bushfire-prone Areas Code overlays and is zoned General Residential and Rural.



Image 5: Council zoning and overlays

Red:	General Residential
Cream:	Rural
Green hatch:	Natural Assets Code
Whole site:	Bushfire-prone Areas Code



## **Fire History:**

From the Fire History overlay detailed within *The LIST* map imagery, three bushfire events are mapped within a 2 km range of the site.

Year	Name	Area	Cause
1967	1967 Fire	±200,000 ha	Unknown
2006	Mt Direction	±25 ha	Unknown
2013	Mt Direction MTNRA001S	±456 ha	Planned



Image 6: Bushfire History (Source: The LIST)

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#### LARK & CREESE



#### 4. PROPOSED DEVELOPMENT:

A 3 lot and balance area subdivision is proposed for the site. Access to the new residential lots will be from a new road extension on Alana Court with new water, sewer and stormwater services to be installed.

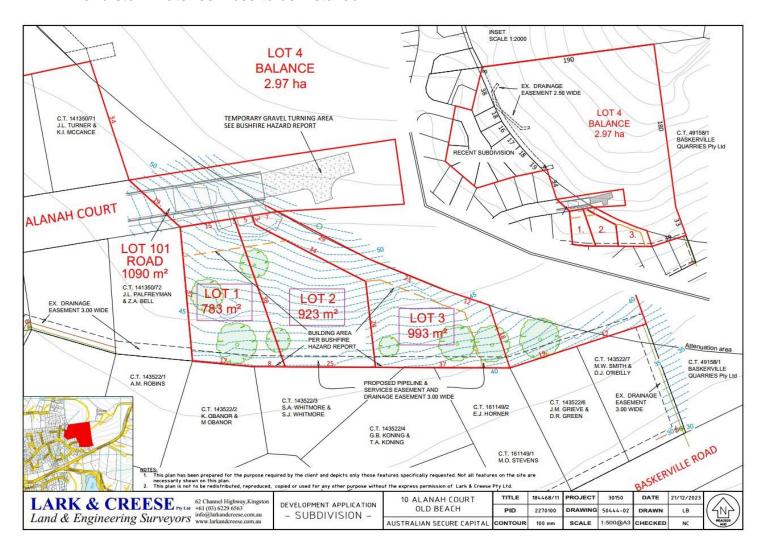


Image 7: Subdivision layout



#### 5. BUSHFIRE ATTACK LEVEL:

Fire Danger Index (FDI): The Fire Index Rating for Tasmania is adopted as 50.

## **Vegetation Assessment:**

Following assessment of the characteristics of the site, the vegetation types, separation distances from development site and slope under the vegetation have been identified as shown in Table 1 below:

Lot N°	Direction:	Vegetation type:	Distance (m):	Slope:
	North	Forest	0-100	17° up
1	East	Forest	0-100	3° down
ı	South	LTV	0-100	11° down
	West:	LTV	0-100	16° down
	North	Forest	0-60	17° up
		Grass	60-100	10° up
2	East	Forest	0-100	5° down
2	South	LTV	0-100	11° down
	West	Forest	0-53	Level
		LTV	53-100	16° down
	North	Forest	0-60	18° up
		Grassland	60-100	14° up
3	East	Forest	0-100	3° down
3	South	LTV	0-100	11° down
	West	Forest	0-60	Level
		LTV	60-100	16° down
	North:	Forest	0-100	11° up
	Northeast:	Forest	0-20	12° up
		Grassland	20-55	13° up
		Forest	55-100	14° up
4	East:	Forest	0-100	Level
	South:	Forest	0-20	9° down
		LTV	20-100	
		Forest	55-65	
	West:	Grassland	0-10	8° down
		LTV	10-100	

Table 1: Site Assessment



NOTE: The vegetation identified above has been assessed in consideration of *Table 2.3* and *Figures 2.4 (A)-(H), AS 3959:2018* as follows

The majority of the vegetation within the subject property consisted of eucalypts, 5-15 metres in height, with an understory of smaller trees and shrubs with a foliage coverage of >30% and is assessed in accordance with *Figure 2.4(B)* as *Open Forest A-03* resulting in a vegetation classification of **A: Forest**. The vegetation within the reminder of the allotment consisted of grasses that were more than 100 mm in height and have been assessed in accordance with *Figure 2.4(H)* as *Closed Tussock Grassland G-21* resulting in a vegetation classification of **G: Grassland**.

To the south and west of the site was an extensive area of well-established residential allotments and several roads. The residential allotments included dwellings, sheds, accesses, and gardens. Baskerville Road to the south included grassed nature strips and a bitumen carriageway. Childs Drive, Clives Avenue, Alanah Court, Shelmore Drive, Tandara Court, and Wigram Court, to the west of the site consisted of grassed nature strips, grassed nature strips, and bitumen carriageways. As such the vegetation to the south and west has been classified as **Low Threat Vegetation** (LTV) in accordance with *Part 2.2.3.2 (e) & (f), AS* 3959:2018.



## **Vegetation Classification:**

In consideration of vegetation classifications under *Table 2.3* and *Figures 2.4 (A)-(H), AS 3959:2018* and as detailed above, the predominant vegetation, separation distances from development site and slope under the classified vegetation is assessed as shown in Table 2 below:

Direction:	Vegetation Type:	Distance (m):	Slope:	Exclusions:
	<u> </u>	LOT 1		
North:	A: Forest	0-100	17° up	No
East:	A: Forest	0-100	3° down	No
South:	LTV	0-100	11° down	2.2.3.2 (e) & (f)
West:	LTV	0-100	16° down	2.2.3.2 (e) & (f)
		LOT 2		
North:	A: Forest G: Grassland	0-60 60-100	17° up 10° up	No No
East:	A: Forest	0-100	5° down	No
South:	LTV	0-100	11° down	2.2.3.2 (e) & (f)
West:	A: Forest LTV	0-28 28-100	Level 16° down	No 2.2.3.2 (e) & (f)
		LOT 3		
North:	A: Forest G: Grassland	0-60 60-100	18° up 14° up	No No
East:	A: Forest	0-100	3° down	No
South:	LTV	0-100	11° down	2.2.3.2 (e) & (f)
West:	A: Forest LTV	0-60 60-100	Level 16° down	No 2.2.3.2 (e) & (f)
		LOT 4		
North:	A: Forest	0-100	11° up	No
East:	A: Forest	0-100	Level	No
South:	A: Forest LTV A: Forest	0-20 20-100 55-65	9° down	No 2.2.3.2 (e) & (f) No
West:	G: Grassland LTV	0-10 10-100	8° down	No 2.2.3.2 (e) & (f)



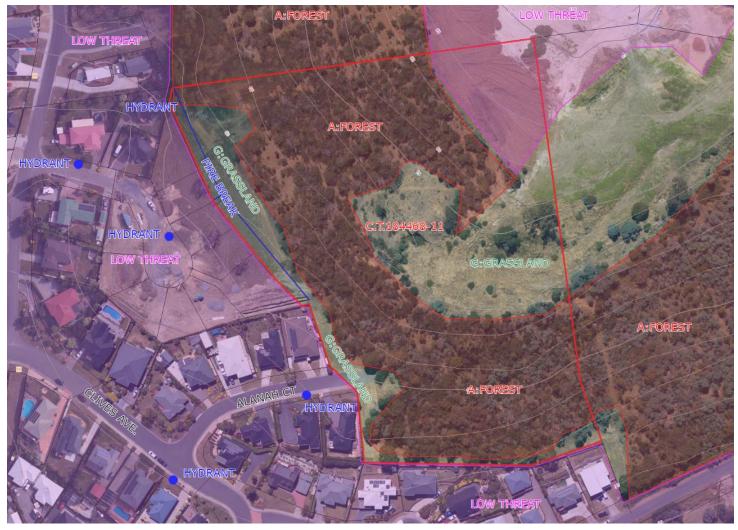


Image 8: Aerial image of assessed vegetation (Source The LIST)





Image 9: Predominate vegetation to the north of site - A: Forest



Image 10: Predominate vegetation to the east of site - A: Forest

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Image 11: Predominate vegetation to the south of site – Low Threat Vegetation



Image 12: Predominate vegetation to the west of site – **Low Threat Vegetation**16

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## **Bushfire Attack Level (BAL):**

Based on the predominant vegetation detailed above, and the separation distances available between the predominant vegetation and the development, the BAL applicable for a compliant building area within each lot has been determined from *Table 2.6, AS 3959:2018* as follows:

LOT N°	Direction	Vegetation Classification	Slope	HMA per Table 2.6	Boundary setback
	North	A: Forest	17° up	23-<32 m	8m ***
	East	A: Forest	3° d	27-<38 m	0m **
1	South	LTV	11° d	N/A	0m
	West	LTV	16° d	N/A	0m
	North	A: Forest	17° up	23-<32 m	8m ***
2	East	A: Forest	5° d	34-<46 m	0m **
2	South	LTV	11° d	N/A	0m
	West	A: Forest	Level	23-<32 m	0m **
	North	A: Forest	18° up	23-<32 m	4m ++
3	East	A: Forest	3° d	27-<38 m	7m ++
3	South	LTV	11° d	N/A	0m
	West	A: Forest	Level	23-<32 m	0m **
4	North	A: Forest	11° up	23-<32 m	23m <<
	East	A: Forest	Level	23-<32 m	23m <<
	South	A: Forest	9° d	34-<46 m	0m **
	West	G: Grassland	8° d	13-<19 m	0m

Table 2: Assessed Bushfire Attack Level for each lot

<< Lot 4 is the balance area and has numerous possible building areas. This site currently has limited development potential due to its Rural zoning and disused

<sup>\*\*</sup> Boundary setbacks are 0m as a result of clearing of the HMA required to the north and east for Lot 3 and within Lots 1, 2 & 3.

<sup>\*\*\*</sup> Boundary setback of 8m is required as a result of the bushfire threat associated with the vegetation on the northern side of the road within Lot 4.

<sup>++</sup> A 20m HMA is to be established outside boundaries of Lot 3 to north and east to provide minimum setback to classified vegetation. A Part 5 Agreement will be required to ensure on-going management of this area.



quarry site in the east with the most likely building area to be as shown on the BHMP. This land is likely to be subdivided in the future subject to rezoning. Any future building areas will be considered at that time.



#### 6. COMPLIANCE:

The site has been assessed as being within 100 metres of bushfire prone vegetation and compliance is assessed against the provisions of *C13.0*, *Bushfire Prone Areas Code* in the following manner:

## C13.6.1 Provision of hazard management areas:

That subdivision provides for hazard management areas that:

- (a) facilitate an integrated approach between subdivision and subsequent building on a lot;
- (b) provide for sufficient separation of building areas from bushfire-prone vegetation to reduce the radiant heat levels, direct flame attack and ember attack at the building area; and
- (c) provide protection for lots at any stage of a staged subdivision.

Acceptable Solutions			
TFS or an accredited person certifies that there is an insufficient increase in			
risk from bushfire to warrant the provision of hazard management areas as part			
of a subdivision; or			
The proposed plan of subdivision;			
(i) Shows all lots that are within of partly within a bushfire-prone area,			
including those developed at each stage of a staged subdivision;			
(ii) Shows the building area for each lot;			
(iii) Shows hazard management areas between bushfire-prone vegetation			
and each building area that have dimensions equal to or greater than,			
the separation distances required for BAL-19 in Table 2.6 of Australian			
Standard AS 3959:2018 Construction of buildings in bushfire-prone			
areas; and			
(iv) Is accompanied by a bushfire hazard management plan that			
addresses all the individual lots and that is certified by the TFS or			
accredited person, showing hazard management areas equal to , or			
greater than, the separation distances required for BAL-19 in Table			
2.6 of Australian Standard AS 3959:2018 Construction of buildings in			
bushfire-prone areas; and			
If hazard management areas are to be located on land external to the proposed			
subdivision the application is accompanied by the written consent of the owner			
of the land to enter into an agreement under section 71 of the Act that will be			
registered on the title of the neighbouring property providing for the affected			
land to be managed in accordance with the bushfire hazard management plan.			



The proposed subdivision has been assessed as being compliant with the Acceptable Solutions (b) as follows.

- (i) The plan of subdivision shows all lots within or partly within a bushfire-prone area.
- (ii) The plan of subdivision shows compliant building areas for all proposed allotments.
- (iii) Each lot is capable of complying with the hazard management requirements of at least those required for BAL-19.
- (iv) The attached hazard management plan shows hazard management areas for each lot that are equal to or greater than the distances required for BAL-19.

Lots assessed as **BAL-19** are:

LOTS: 1 - 4

Compliance with the requirements of *C13.6.1(b)(iii)* is dependent on the establishment of a Hazard Management Area within Lot 4 to provide sufficient separation between the building areas on Lots 1, 2 & 3 and the classified vegetation. In accordance with *C13.6.1 A1(c)*, a Part 5 Agreement is to be registered on the titles to the lots to ensure the establishment and maintenance of this HMA in a low fuel condition. Establishment of this HMA is the responsibility of the developer and is to occur prior to the Council sealing of the Plan of Survey. On-going management is to be the responsibility of the owner of Lot 4. Provisions are to be contained within the Part 5 to permit dispensation of these requirements should that portion of Lot 4 be subdivided into residential allotments, or permanently maintained on a low fuel condition as a result of an approved use on the site.



Hazard Management Area requirements (boundary setbacks)				
Direction	North	East	South	West
Lot 1	8m	0m	0m	0m
Lot 2	8m	0m	0m	0m
Lot 3	4m	7m	0m	0m
Lot 4	23m	23m	0m	0m
HMA establishment recommendations  Ongoing	<ul> <li>patios, drivewa</li> <li>Locating dams on the bushfire</li> <li>Providing head dwelling such shrubs and sm</li> <li>Store flammab are stored awa</li> <li>Replace highly Tasmanian Fir resisting garde</li> <li>Provided sepa greater than 2 groups of sign screen a dwell</li> <li>Trim lower braground level.</li> <li>Strips of veget of the site or of as an ember tree.</li> <li>Removal of greaters</li> </ul>	ay, lawns etc. s, orchards, vegeta e prone side of the le s shields and embe as non-flammable hall tress, ble materials such a ay from the dwelling of flammable vegeta e Service web site ( en plants. aration between signon metres in width, hifficant trees. Note ling from windborne anches of retained attion less than 20 n other areas of bushfrap, wind breaks etc ound fuels such as	ble garden, effluen building. It trap on the bushfite fencing, hedges, as wood piles, fuels a	lling such as paths, t disposal areas etc re prone side of the separated garden and rubbish heaps hability species. See all publications - Fire that groups are no metres of the other of some trees can not within 20 metres on may be beneficial branches etc.
Ongoing Management practices	<ul> <li>Slash or mow grasses to less than 100 mm.</li> <li>Remove dead and fallen vegetation including branches, bark and leaves regularly.</li> <li>Trim any regrowth branches of retained trees within HMA that are less than 2m above ground level.</li> </ul>			



## C13.6.2 Subdivision: Public and fire fighting access

That access roads to, and the layout of roads, tracks and trails, in a subdivision:

- (a) allow safe access and egress for residents, firefighters and emergency service personnel;
- (b) provide access to the bushfire-prone vegetation that enables both property to be defended when under bushfire attack and for hazard management works to be undertaken;
- (c) are designed and constructed to allow for fire appliances to be manoeuvred:
- (d) provide access to water supplies for fire appliances; and
- (e) are designed to allow connectivity, and where needed, offering multiple evacuation points.

A1	Acceptable solutions	
(a)	TFS or an accredited person certifies that there is insufficient increase in risk from bushfire to warrant specific measures for public access in the subdivision for the purposes of fire fighting; or	
(b)	for the purposes of fire fighting; or	

The proposed subdivision has been assessed as being compliant with the Acceptable Solutions (b) as follows.

- (i) The attached plan of subdivision shows the layout of roads, fire trails and the location of the property accesses to the building areas in compliance with *Table C13.1*, *Table C13.2* and *Table C13.3*. Note variation in turning area in accordance with *C13.6.2 P1*.
- (ii) This bushfire hazard report and attached bushfire hazard management area plan has been certified by N.M. Creese, an accredited bushfire practitioner BFP-118, scope 1, 2, 3A, 3B & 3C.

The development requires the construction of a short extension to the Alanah Court carriageway and is to comply with the requirements of *Table C13.1*. A temporary turning head at the end of Alanah Court is installed. Due to site constraints, a 'Y' turning area is proposed in accordance with *C13.6.2 P1*.



(c) Any advice from the TFS

P1	Performance Criteria			
	A proposed plan of subdivision shows access and egress for residents, fire-fighting			
	icles and emergency service personnel to enable protection from bushfires, having			
rega	ard to appropriate design measures, including:			
(a)	A proposed plan of subdivision shows access and egress for residents, fire-fighting			
	vehicles and emergency service personnel to enable protection from bushfires,			
	having regard to:			
	appropriate design measures, including:			
	(i) two way traffic;			
	(ii) all weather surfaces;			
	(iii) height and width of any vegetation clearances;			
	(iv) load capacity;			
	(v) provision of passing bays;			
	(vi) traffic control devices;			
	(vii) geometry, alignment and slope of roads, tracks and trails;			
	(viii) use of through roads to provide for connectivity;			
	(ix) limits on the length of cul-de- sacs and dead-end roads;			
	(x) provision of turning areas;			
	(xi) provision for parking areas;			
	(xii) perimeter access; and			
	(xiii) fire trails; and			
(b)	the provision of access to:			
	(i) bushfire-prone vegetation to permit the undertaking of hazard management			
	works; and			
	(ii) fire fighting water supplies; and			

Due to the limitations associated with slope in the vicinity of the termination of the new road, a variation on the design of the turning area is proposed. A 'Y" design turning area has been designed by the engineer to facilitate a 3 point turn of a standard medium-rigid fire appliance. This area is to be of a compacted gravel formation and lies within the proposed road corridor extension and will be transferred to the Brighton Council in conjunction with the extension of the sealed portion of Alanah Court. Improved separation between the turning area and the unmanaged vegetation on the down-slope side is facilitated through the creation of the HMA within Lot 4 to the east of Lot 1 which is to be maintained in a low fuel condition in accordance with the requirements of this report. The turning area lies within an area proposed for a future subdivision road extending to the east and north (subject to rezoning and Council approval) which will provide for connector roads to land to the north, and additional turning areas.

Tabl	Table C13.1 Standards for Roads			
Elements Requirement		Requirement		
А	Roads	Unless the development standards in the zone require a higher standard, the following apply;  (a) Two-wheel drive, all-weather construction;  (b) Load capacity of at least 20t, including for bridges and culverts:		



(c) Minimum carriageway width is 7m for through road, or
5.5m for dead-end or cul-de-sac road;
(d) Minimum vertical clearance of 4m;
(e) Minimum horizontal clearance of 2m from the edge of the carriageway;
(f) Cross falls of less than 3 degrees (1:20 or 5%);
(g) Maximum gradient of 15 degree (1:3.5 or 28%) for sealed
roads, and 10 degrees (1:5.5 or 18%) for unsealed roads;
(h) Curves have a minimum inner radius or 10m;
<ul><li>(i) Dead-end or cul-de-sac roads are not more than 200m in length unless the carriageway is 7m in width;</li></ul>
(j) Dead-end or cul-de-sac roads have a turning circle with a minimum 12m outer radius; and
(k) Carriageways less then 7m wide have 'No Parking' zones on one side, indicated by a road sign that complies with
Australian Standard AS 1743-2001 road signs- Specifications.

New private accesses must be constructed from the edge of the turning area to the property boundaries of the lots in compliance with *Table C13.2*. Access to the building areas on each lot is less than 30m in length and is to comply with the requirements of *Element A, Table C13.2*. No standards apply.

Should an access exceed 30m in length, access is to comply with the requirements of *Element B, Table C13.2.* Where this occurs, construction of the access to the building area and on-site turning is not required at the time of subdivision however is to be installed at the time of development of a building required to comply with the standards.

Tabl	Table C13.2 Standards for Property Access				
Elen	nents	Requirement			
A	Property access length is less than 30m; or access in not required for a fire appliance to access a firefighting water point	, ,			
В	Property access length is 30m or greater; or access is required for a fire appliance to a fire fighting water point.	(a) All-weather construction; (b) Load capacity of at least 20t, including for			



		<ul> <li>(g) Dips less than 7 degrees (1:8 or 12.5%) entry and exit angles;</li> <li>(h) Curves with a minimum inner radius of 10m;</li> <li>(i) Maximum gradient of 15 degrees (1:3.5 or 28%) for sealed roads, and 10 degrees (1:5.5 or 18%) for unsealed roads; and</li> <li>(j) Terminate with a turning area for fire appliances provided by one of the following;</li> <li>(i) A tuning circle with a minimum outer radius of 10m; or</li> <li>(ii) A property access encircling the building; or</li> <li>(iii) A hammerhead 'T' or 'Y' turning head 4m wide and 8m long.</li> </ul>	
С	Property access length is 200m or greater.	,	
D	Property access length is greater than 30m, and access is provided to 3 or more properties.	The following design and constructions requirements apply to property access:  (a) Complies with requirement b above; and	



## C13.6.3 Provision of water supply for fire fighting purposes

That an adequate, accessible and reliable water supply for the purposes of fire fighting can be demonstrated at the subdivision stage to allow for the protection of life and property associated with the subsequent use and development of bushfire-prone areas.

In a	In areas serviced with reticulated water by the water corporation		
A1	Acceptable solutions		
(a)	TFS or an accredited person certifies that there is an insufficient increase in risk		
	from bushfire to warrant the provision of a water supply for fire fighting purposes;		
(b)	A proposed plan of subdivision showing the layout of fire hydrants, and building		
	areas, is included in a bushfire hazard management plan approved by the TFS or		
	accredited person as being compliant with Table E4; or		
(c)	A bushfire hazard management plan certified by the TFS or an accredited person		
	demonstrates that the provision of water supply for fire fighting purposes is		
	sufficient to manage the risks to property and lives in the event of a bushfire.		

In accordance with *Acceptable Solution A1(b)* all lots are assessed as being within a bushfire prone area and must be provided with a fire fighting supply of water from a reticulated supply in compliance with the provisions of *Table C13.4*, *E1.6.2*, the *Code* as follows:

Ta	Table C13.4 Reticulated water supply for Fire Fighting			
Element		Requirement		
A	Distance between buildings area to be protected and water supply	The following requirements apply:  (a) The building area to be protected must be located within 120m of a fire hydrant; and  (b) The distance must be measured as a hose lay, between the fire fighting water point and the furthest part of the building area.		
В	Design criteria for fire hydrants	The following requirements apply:  (a) Fire hydrant system must be designed and constructed in accordance with TasWater Supplements to Water Supplement to Water Supply Code of Australia WSA 03-2001-3.1 MRWA 2nd Editions; and  (b) Fire hydrants are not installed in parking areas.		
С	Hardstand	A hardstand area for fire appliances must be:  (a) No more the 3m from the hydrant, measured as a hoselay;  (b) No closer than 6m from the building area to be protected;  (c) A minimum width of 3, constructed to the same standard as the carriageway; and  (d) Connected to the property access by a carriageway equivalent to the standard of the property access.		



The building area within each allotment has been identified as being within a 120-metre hose lay of the proposed fire hydrant located in Alanah Court in compliance with *Table C13.4*.



#### 7. CONCLUSIONS & RECOMMENDATIONS:

This Bushfire Hazard Report and Bushfire Hazard Management Plan have been prepared to support application for planning approval for a subdivision at 10 Alanah Court, Old Beach. The report has reviewed the bushfire risks associated with the site, and determined the fire management strategies that must be carried out to ensure the development on the site is at reduced risk from bushfire attack.

Provided the elements detailed in this report are implemented, the development on the site is capable of compliance with AS 3959:2018 and C13.6 Bushfire-Prone Areas Code and any potential bushfire risk to the site is reduced.

The proposed lots have been assessed as compliant with bushfire attack levels (BAL) detailed in Table 2. The Council approval issued for the development should contain conditions requiring that the protective elements defined in this report and *C13.6*, *Bushfire-Prone Areas Code* be implemented during the construction phase. Any new building required to comply with this assessment must be constructed to the bushfire attack level described in Table 2, within the prescribed building areas noted on the Bushfire Hazard Management Plan. Should the extent or classification of the bushfire prone vegetation surrounding the site alters from that assessed by this report, building on the lots affected by this variation may be constructed to a lower level subject to the preparation of a revised assessment.

Lot No.	Compliant BAL
1 - 4	BAL-19

Table 3: Compliant BAL for each lot

- Each lot contains a building area with minimum setbacks required for BAL-19 in accordance with C13.6.1 Provision of hazard management areas. Hazard Management Areas are to be established at the time of subdivision with on-going management to be the responsibility of each lot owner. A Part 5 Agreement is to be established to require management of the HMA within Lot 4 to the east and north of Lot 3 in a low fuel condition. This area is to be established at the time of subdivision with on-going management to be the responsibility of the owner of Lot 4.
- The new public road is to comply with the requirements of *Table 13.1 Standards* for Road. This is to include a temporary turning area at the end of Alanah Court. Private accesses are to be constructed from Alanah Court to the boundary of each property in accordance with *Table C13.2 Property Access*.
- A fire hydrant is proposed within the Alanah Court Road Reserve and is to comply with the requirements of *Table C13.4. Reticulated water supply for fire fighting*.

All works required by this report are to be completed prior to the Council sealing the final Plan of Survey unless noted otherwise.



Although not mandatory, any increase in the construction standards above the assessed Bushfire Attack Level will afford improved protection from bushfire and this should be considered by the owner, designer and/or builder prior to construction commencing.

Hazard Management Areas must be established and maintained in a minimal fuel condition in accordance with this plan and the TFS guidelines. It is the owner's responsibility to ensure the long-term maintenance of the hazard management areas in accordance with the requirements of this report.

This report does not recommend or endorse the removal of any vegetation within or adjoining the site for the purpose of bushfire protection without the explicit approval of the local authority.

N M Creese Bushfire Hazard Practitioner BFP-118 Scope 1, 2, 3A, 3B & 3C





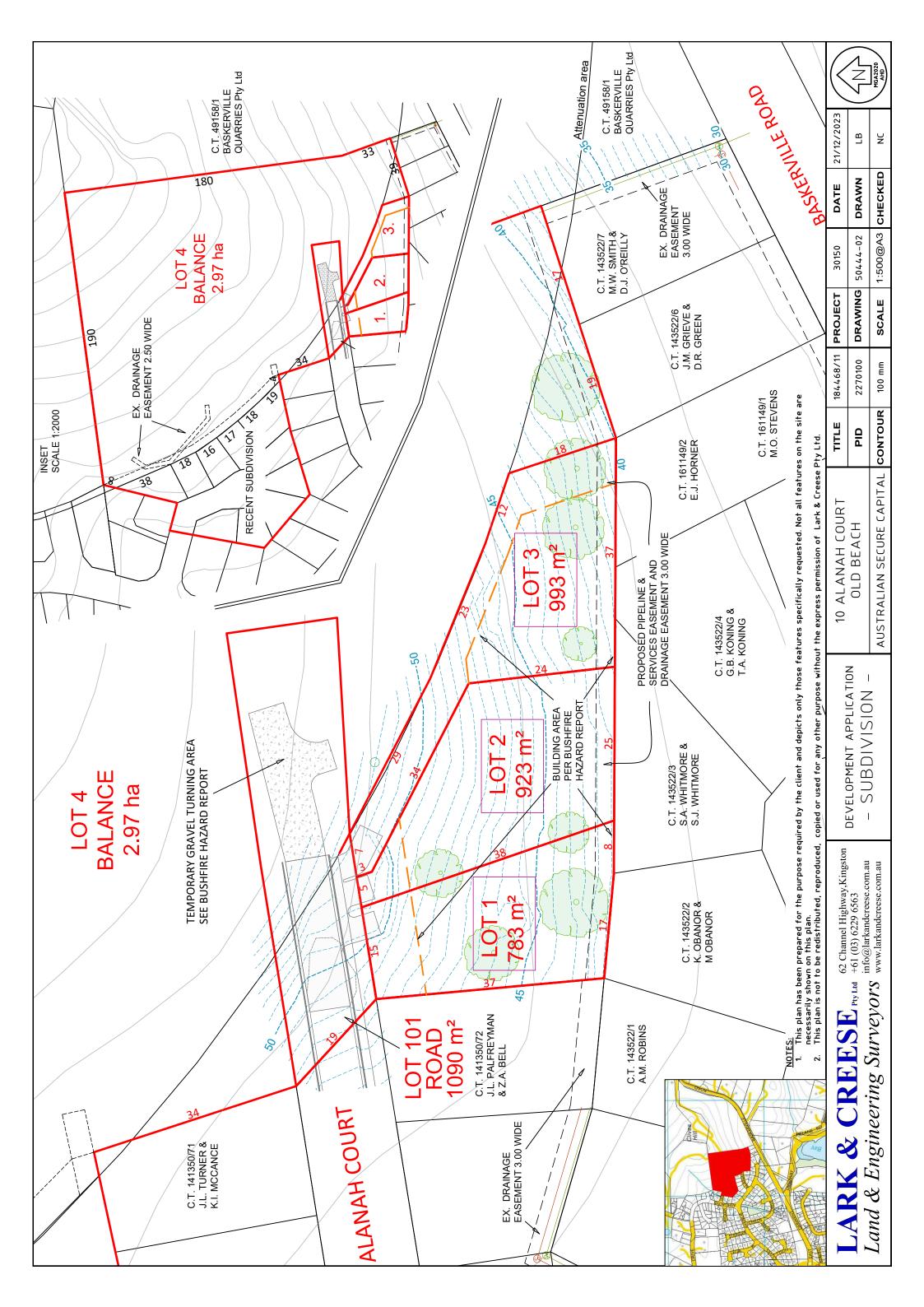
## 8. REFERENCES:

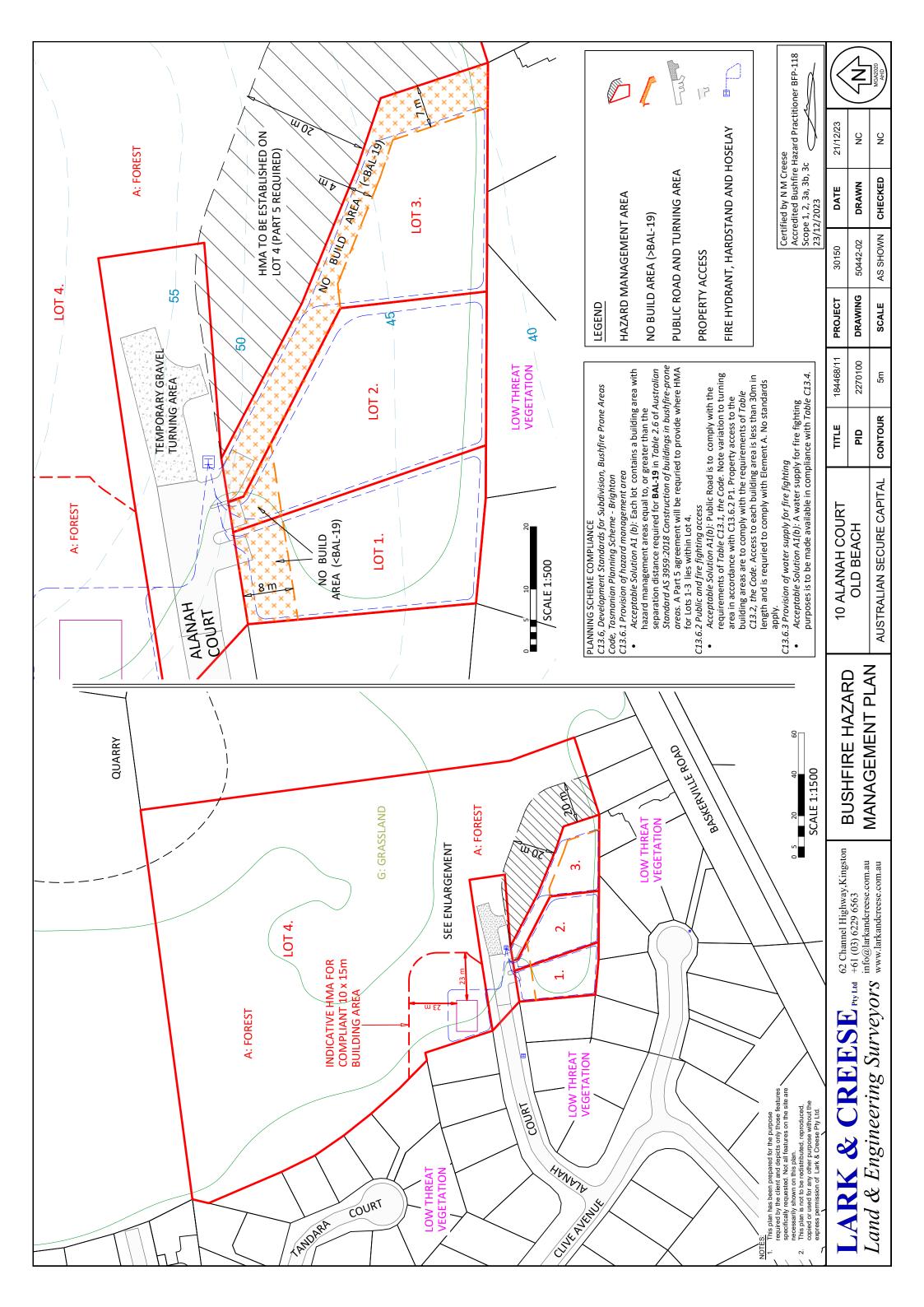
- AS 3959:2018 Construction of Buildings in Bushfire Prone Areas.
- Tasmanian Planning Scheme Brighton.
- The LIST Department of Primary Industry Parks Water & Environment.



## 9. GLOSSARY

AS 3959:2018	Australian Standards AS 3959:2018 Construction of buildings in bushfire-prone areas.
BAL (Bushfire Attack Level)	A means of measuring the severity of a building's potential exposure to ember attack, radiant heat and direct flame contact, using increments of radiant heat expressed in kilowatts per metre squared, and the basis for establishing the requirements for construction to improve protection of building elements from attack by bushfire. The following BAL levels, based on heat flux exposure threshold are used within AS3959:2018; BAL-LOW, BAL-12.5, BAL-19, BAL-29, BAL-40, BAL-FZ.
Bushfire	An unplanned fire burning vegetation.
Bushfire Hazard Management Plan	A plan showing means of protection from bushfire in a form approved in writing by the Chief Officer.
Bushfire-Prone Area	An area that is subject to, or likely to be subject to, bushfire attack. Land that has been designated under legislation; or Has been identified under environmental planning instrument, development control plan or
	in the course of processing and determining a development application.
Carriageway (also vehicular access)	The section of the road formation which is used by traffic, and includes all the area of the traffic lane pavement together with the formed shoulder.
Classified vegetation	Vegetation that has been classified in accordance with Clause 2.2.3 of AS3959:2018.
Distance to	The distance between the building, or building area to the classified vegetation.
FDI (Fire Danger Index)	The chance of a fire starting, its rate of spread, its intensity and the difficulty of its suppression, according to various combinations of air temperature, relative humidity, wind speed and both long- and short-term drought effects.
Fire Fighting Water Point	Means the point where a fire appliance is able to connect to a water supply for fire fighting purposes. This includes a coupling in the case of a fire hydrant, offtake or outlet, or the minimum water level in the case of a static water body (including a dam, lake or pool).
Gradient under	The slope of the ground under the classified vegetation.
Hazard Management Area	The area between a habitable building or building area and bushfire-prone vegetation, which provides access to a fire front for fire fighting, which is maintained in a minimal fuel condition and in which there are no other hazards present which will significantly contribute to the spread of a bushfire.
Hose lay	The distance between two points established by a fire hose laid out on the ground, inclusive of obstructions.
Predominate vegetation	The vegetation that poses the greatest bushfire threat to the development site.
Water supply - Reticulated (Fire hydrant)	An assembly installed on a branch from a water pipeline, which provides a valved outlet to permit a supply of water to be taken from the pipeline for fire fighting.
Water supply - Static	Water stored on a tank, swimming pool, dam, or lake, that is available for fire fighting purposes at all times.





## **BUSHFIRE-PRONE AREAS CODE**

# CERTIFICATE<sup>1</sup> UNDER S51(2)(d) LAND USE PLANNING AND APPROVALS ACT 1993

## 1. Land to which certificate applies

The subject site includes property that is proposed for use and development and includes all properties upon which works are proposed for bushfire protection purposes.

Street address: 10 ALANAH COURT, OLD BEACH

Certificate of Title / PID: C.T. 184468/11 PID 2270100

## 2. Proposed Use or Development

Description of proposed Use and Development:

**SUBDIVISON** 

**Applicable Planning Scheme:** 

TASMANIAN PLANNING SCHEME - BRIGHTON

## 3. Documents relied upon

This certificate relates to the following documents:

Title	Author	Date	Version
SUBDIVISON PROPOSAL	Lark & Creese Pty Ltd	21/12/2023	50444-02
BUSHFIRE HAZARD REPORT	N.M. Creese	21/12/2023	50442-02

<sup>&</sup>lt;sup>1</sup> This document is the approved form of certification for this purpose and must not be altered from its original form.

4	Matrica		Certificate	
4.	nature	OT	Certificat	e

The following requirements are applicable to the proposed use and development:

E1.4 / C13.4 – Use or development exempt from this Code	
Compliance test	Compliance Requirement
E1.4(a) / C13.4.1(a)	Insufficient increase in risk

E1.5.1 / C13.5.1 – Vulnerable Uses	
Acceptable Solution	Compliance Requirement
E1.5.1 P1 / C13.5.1 P1	Planning authority discretion required. A proposal cannot be certified as compliant with P1.
E1.5.1 A2 / C13.5.1 A2	Emergency management strategy
E1.5.1 A3 / C13.5.1 A2	Bushfire hazard management plan

E1.5.2 / C13.5.2 – Hazardous Uses	
Acceptable Solution	Compliance Requirement
E1.5.2 P1 / C13.5.2 P1	Planning authority discretion required. A proposal cannot be certified as compliant with P1.
E1.5.2 A2 / C13.5.2 A2	Emergency management strategy
E1.5.2 A3 / C13.5.2 A3	Bushfire hazard management plan

	E1.6.1 / C13.6.1 Subdivision: Provision of hazard management areas		
	Acceptable Solution	Compliance Requirement	
	E1.6.1 P1 / C13.6.1 P1	Planning authority discretion required. A proposal cannot be certified as compliant with P1.	
	E1.6.1 A1 (a) / C13.6.1 A1(a)	Insufficient increase in risk	
$\square$	E1.6.1 A1 (b) / C13.6.1 A1(b)	Provides BAL-19 for all lots (including any lot designated as 'balance')	
	E1.6.1 A1(c) / C13.6.1 A1(c)	Consent for Part 5 Agreement	

	E1.6.2 / C13.6.2 Subdivision: Public and fire fighting access		
	Acceptable Solution	Compliance Requirement	
Ø	E1.6.2 P1 / C13.6.2 P1	Planning authority discretion required. A proposal cannot be certified as compliant with P1. (TURNING AREA ONLY)	
	E1.6.2 A1 (a) / C13.6.2 A1 (a)	Insufficient increase in risk	
Ø	E1.6.2 A1 (b) / C13.6.2 A1 (b)	Access complies with relevant Tables (EXCLUDING TURNING AREA)	

	E1.6.3 / C13.1.6.3 Subdivision: Provision of water supply for fire fighting purposes				
	Acceptable Solution	Compliance Requirement			
	E1.6.3 A1 (a) / C13.6.3 A1 (a)	Insufficient increase in risk			
$\square$	E1.6.3 A1 (b) / C13.6.3 A1 (b)	Reticulated water supply complies with relevant Table			
	E1.6.3 A1 (c) / C13.6.3 A1 (c)	Water supply consistent with the objective			
	E1.6.3 A2 (a) / C13.6.3 A2 (a)	Insufficient increase in risk			
	E1.6.3 A2 (b) / C13.6.3 A2 (b)	Static water supply complies with relevant Table			
	E1.6.3 A2 (c) / C13.6.3 A2 (c)	Static water supply consistent with the objective			

## 5. Bushfire Hazard Practitioner Phone No: 62296563 NICHOLAS MARK CREESE Name: **62 CHANNEL HIGHWAY Postal Email** info@larkandcreese.com.au Address: Address: KINGSTON, TAS, 7050 **Accreditation No:** 1, 2, 3A, 3B, 3C BFP - 118 Scope: 6. Certification I certify that in accordance with the authority given under Part 4A of the Fire Service Act 1979 that the proposed use and development: Is exempt from the requirement Bushfire-Prone Areas Code because, having regard to the objective of all applicable standards in the Code, there is considered to be an insufficient increase in risk to the use or development from bushfire to warrant any specific bushfire protection measures, or The Bushfire Hazard Management Plan/s identified in Section 3 of this certificate $\mathbf{V}$ is/are in accordance with the Chief Officer's requirements and compliant with the relevant Acceptable Solutions identified in Section 4 of this Certificate.

21/12/2023

50442-02

Date:

Certificate

Number:

(for Practitioner Use only)

N.M. Creese

Signed: certifier

Name:



## **Amended Submission to Planning Authority Notice**

Council Planning Permit No.	SA 2023 / 00019		Council notice date	31/07/2023		
TasWater details						
TasWater Reference No.	TWDA 2023/01014-BTN		Date of response Amended date	28/02/2024 18/06/2024		
TasWater Contact  Jake Walley  Phone No.		0467 625 805				
Response issued to						
Council name	BRIGHTON COUNCIL					
Contact details	development@brighton.tas.gov.au					
Development details						
Address	10 ALANAH CT, OLD BEACH		Property ID (PID)	9352107		
Description of development	Subdivision - 3 Lots + Balance (CT 184468/11)					

#### Schedule of drawings/documents

Prepared by	Drawing/document No.	Revision No.	Date of Issue
Integral Consulting Engineers	22190 Sheet C03b	E	21/05/2024

#### **Conditions**

Pursuant to the *Water and Sewerage Industry Act* 2008 (TAS) Section 56P(1) TasWater imposes the following conditions on the permit for this application:

#### **CONNECTIONS, METERING & BACKFLOW**

- 1. A suitably sized water supply with metered connection and sewerage system and connection to each lot of the development must be designed and constructed to TasWater's satisfaction and be in accordance with any other conditions in this permit.
- 2. Any removal/supply and installation of water meters and/or the removal of redundant and/or installation of new and modified property service connections must be carried out by TasWater at the developer's cost.
- 3. Prior to commencing construction of the subdivision/use of the development, any water connection utilised for construction/the development must have a backflow prevention device and water meter installed, to the satisfaction of TasWater.

#### **ASSET CREATION & INFRASTRUCTURE WORKS**

- 4. Plans submitted with the application for Engineering Design Approval must, to the satisfaction of TasWater show, all existing, redundant and/or proposed property services and mains.
- 5. Prior to applying for a Permit to Construct new infrastructure the developer must obtain from TasWater Engineering Design Approval for new TasWater infrastructure. The application for Engineering Design Approval must include engineering design plans prepared by a suitably qualified person showing the hydraulic servicing requirements for water and sewerage to TasWater's satisfaction.
- 6. Prior to works commencing, a Permit to Construct must be applied for and issued by TasWater. All infrastructure works must be inspected by TasWater and be to TasWater's satisfaction.
- 7. In addition to any other conditions in this permit, all works must be constructed under the supervision of a suitably qualified person in accordance with TasWater's requirements.
- 8. Prior to the issue of a Certificate of Water and sewerage Compliance (Building and/or Plumbing) all



additions, extensions, alterations or upgrades to TasWater's water and sewerage infrastructure required to service the development, are to be completed generally as shown on, and in accordance with, the plans listed in the schedule of drawings/documents, and are to be constructed at the expense of the developer to the satisfaction of TasWater, with live connections performed by TasWater.

- 9. After testing/disinfection, to TasWater's requirements, of newly created works, the developer must apply to TasWater for connection of these works to existing TasWater infrastructure, at the developer's cost.
- 10. At practical completion of the water and sewerage works and prior to applying to TasWater for a Certificate of Water and Sewerage Compliance (Building and/or Plumbing), the developer must obtain a Certificate of Practical Completion from TasWater for the works that will be transferred to TasWater. To obtain a Certificate of Practical Completion:
  - a. Written confirmation from the supervising suitably qualified person certifying that the works have been constructed in accordance with the TasWater approved plans and specifications and that the appropriate level of workmanship has been achieved.
  - b. A request for a joint on-site inspection with TasWater's authorised representative must be made.
  - c. Security for the twelve (12) month defects liability period to the value of 10% of the works must be lodged with TasWater. This security must be in the form of a bank guarantee.
  - d. Work As Constructed drawings and documentation must be prepared by a suitably qualified person to TasWater's satisfaction and forwarded to TasWater.

Upon TasWater issuing a Certificate of Practical Completion, the newly constructed infrastructure is deemed to have transferred to TasWater.

- 11. After the Certificate of Practical Completion has been issued, a 12-month defects liability period applies to this infrastructure. During this period all defects must be rectified at the developer's cost and to the satisfaction of TasWater. A further 12-month defects liability period may be applied to defects after rectification. TasWater may, at its discretion, undertake rectification of any defects at the developer's cost. Upon completion, of the defects liability period the developer must request TasWater to issue a "Certificate of Final Acceptance". TasWater will release any security held for the defect's liability period.
- 12. The developer must take all precautions to protect existing TasWater infrastructure. Any damage caused to existing TasWater infrastructure during the construction period must be promptly reported to TasWater and repaired by TasWater at the developer's cost.
- 13. Ground levels over the TasWater assets and/or easements must not be altered without the written approval of TasWater.
- 14. A construction management plan must be submitted with the application for TasWater Engineering Design Approval. The construction management plan must detail how the new TasWater infrastructure will be constructed while maintaining current levels of services provided by TasWater to the community. The construction plan must also include a risk assessment and contingency plans covering major risks to TasWater during any works. The construction plan must be to the satisfaction of TasWater prior to TasWater's Engineering Design Approval being issued.

#### FINAL PLANS, EASEMENTS & ENDORSEMENTS

15. Prior to the Sealing of the Final Plan of Survey, a Consent to Register a Legal Document must be obtained from TasWater as evidence of compliance with these conditions when application for sealing is made.



<u>Advice:</u> Council will refer the Final Plan of Survey to TasWater requesting Consent to Register a Legal Document be issued directly to them on behalf of the applicant.

- 16. Pipeline easements, to TasWater's satisfaction, must be created over any existing or proposed TasWater infrastructure and be in accordance with TasWater's standard pipeline easement conditions.
- 17. Prior to the issue of a TasWater Consent to Register a Legal Document, the applicant must submit a .dwg file, prepared by a suitably qualified person to TasWater's satisfaction, showing:
  - a. the exact location of the existing water/sewerage infrastructure,
  - b. the easement protecting that infrastructure.

The developer must locate the existing TasWater infrastructure and clearly show it on the .dwg file. Existing TasWater infrastructure may be located by a surveyor and/or a private contractor engaged at the developers cost.

#### **DEVELOPMENT ASSESSMENT FEES**

18. The applicant or landowner as the case may be, must pay a development assessment fee of \$389.86 and a Consent to Register a Legal Document fee of \$248.30 to TasWater, as approved by the Economic Regulator and the fee will be indexed, until the date paid to TasWater.

The payment is required within 30 days of the issue of an invoice by TasWater.

#### **Advice**

#### General

For information on TasWater development standards, please visit <a href="https://www.taswater.com.au/building-and-development/technical-standards">https://www.taswater.com.au/building-and-development/technical-standards</a>

For application forms please visit <a href="https://www.taswater.com.au/building-and-development/development-application-form">https://www.taswater.com.au/building-and-development/development-application-form</a>

#### **Service Locations**

Please note that the developer is responsible for arranging to locate the existing TasWater infrastructure and clearly showing it on the drawings. Existing TasWater infrastructure may be located by a surveyor and/or a private contractor engaged at the developers cost to locate the infrastructure.

- (a) A permit is required to work within TasWater's easements or in the vicinity of its infrastructure. Further information can be obtained from TasWater.
- (b) TasWater has listed a number of service providers who can provide asset detection and location services should you require it. Visit <a href="https://www.taswater.com.au/building-and-development/service-locations">https://www.taswater.com.au/building-and-development/service-locations</a> for a list of companies.
- (c) Sewer drainage plans or Inspection Openings (IO) for residential properties are available from your local council.

NOTE: In accordance with the WATER AND SEWERAGE INDUSTRY ACT 2008 - SECT 56ZB A regulated entity may charge a person for the reasonable cost of –

- (a) a meter; and
- (b) installing a meter.

#### **Declaration**

The drawings/documents and conditions stated above constitute TasWater's Submission to Planning Authority Notice.

#### **TasWater Contact Details**



Phone	13 6992	Email	development@taswater.com.au
Mail	GPO Box 1393 Hobart TAS 7001	Web	www.taswater.com.au